

# Theory of Structures - I

Chapter 5. Influence Lines for  
Simple Structures [Part III of III]

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## 5.9 Determination of Reactions, BM, and SF from ILDs for Different Loadings

In lecture 8, we have learned how to determine the Influence lines and thus ILDs for support reactions, SF and BM at a given section for different types of beams as a unit load moves along its span.

In this lecture, we learn to use the ILDs to find the value of support reactions, shear force, and bending moment at a given section of a beam with given loading.

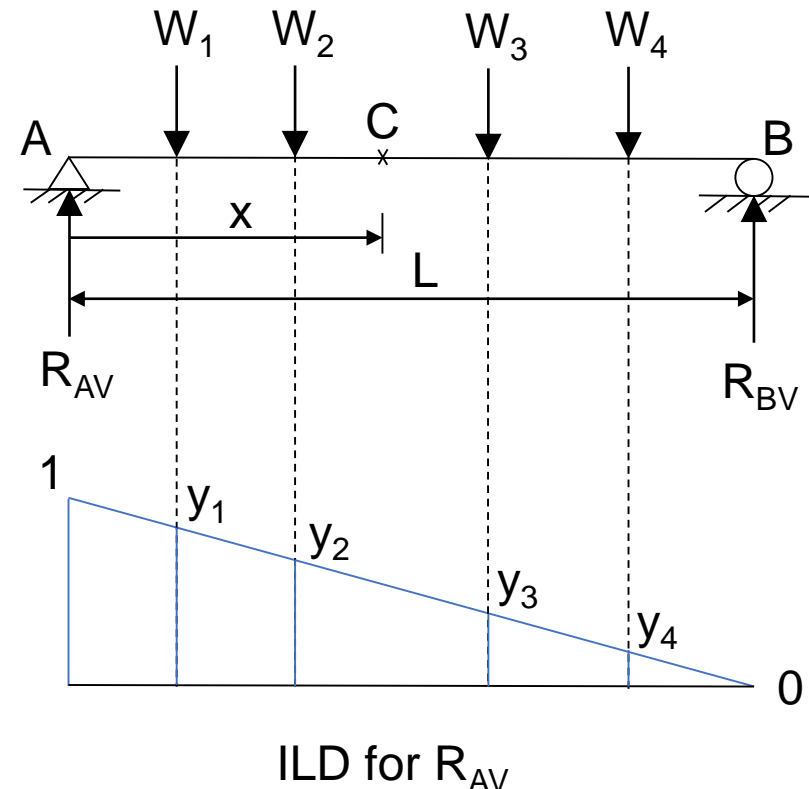
## 5.9 Determination of Reactions, BM, and SF from ILDs for Different Loadings

### Use of ILD (Point loads)

Let us consider a simply supported beam AB subjected to 4 concentrated loads  $W_1$ ,  $W_2$ ,  $W_3$ , and  $W_4$ , for which we calculate the support reactions  $R_{AV}$ ,  $R_{BV}$ , SF and BM at section C of the beam.

We have, ILD for  $R_{AV}$  for simply supported beam as shown in the adjacent figure.

Let  $y_1$ ,  $y_2$ ,  $y_3$ , and  $y_4$  be ordinates of ILD for  $R_{AV}$  at load points  $W_1$ ,  $W_2$ ,  $W_3$ , and  $W_4$ , respectively.



## 5.9 Determination of Reactions, BM, and SF from ILDs for Different Loadings

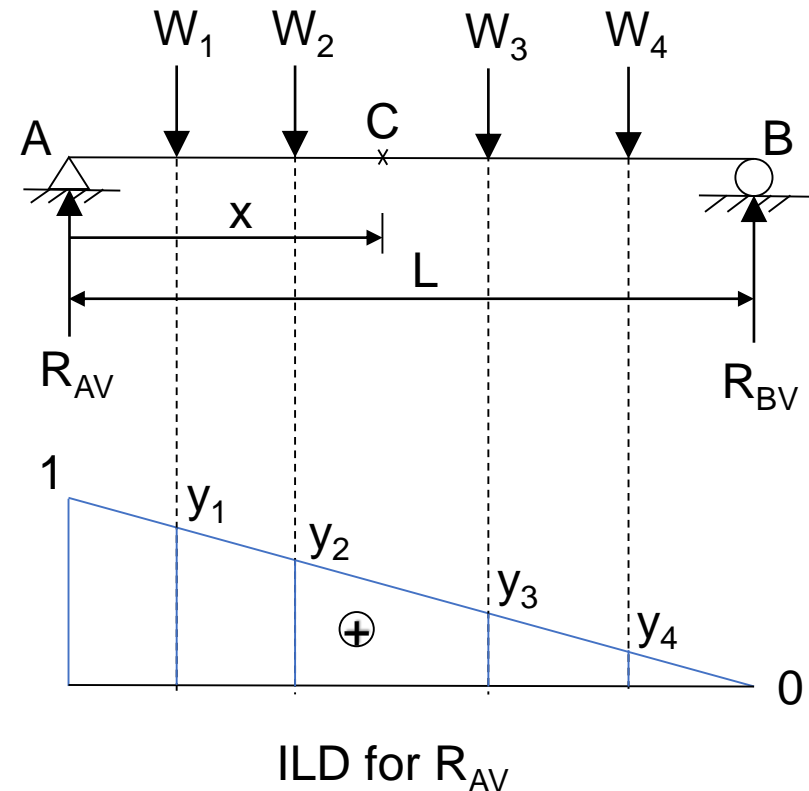
### Use of ILD (Point loads)

Let  $y_1$ ,  $y_2$ ,  $y_3$ , and  $y_4$  be ordinates of ILD for  $R_{AV}$  at load points  $W_1$ ,  $W_2$ ,  $W_3$ , and  $W_4$ , respectively.

Then,

$$R_{AV} \text{ due to the given loadings} \\ = W_1 * y_1 + W_2 * y_2 + W_3 * y_3 + W_4 * y_4$$

**Note:** Take into consideration the signs (+ve or -ve) of the ordinates as well.



## 5.9 Determination of Reactions, BM, and SF from ILDs for Different Loadings

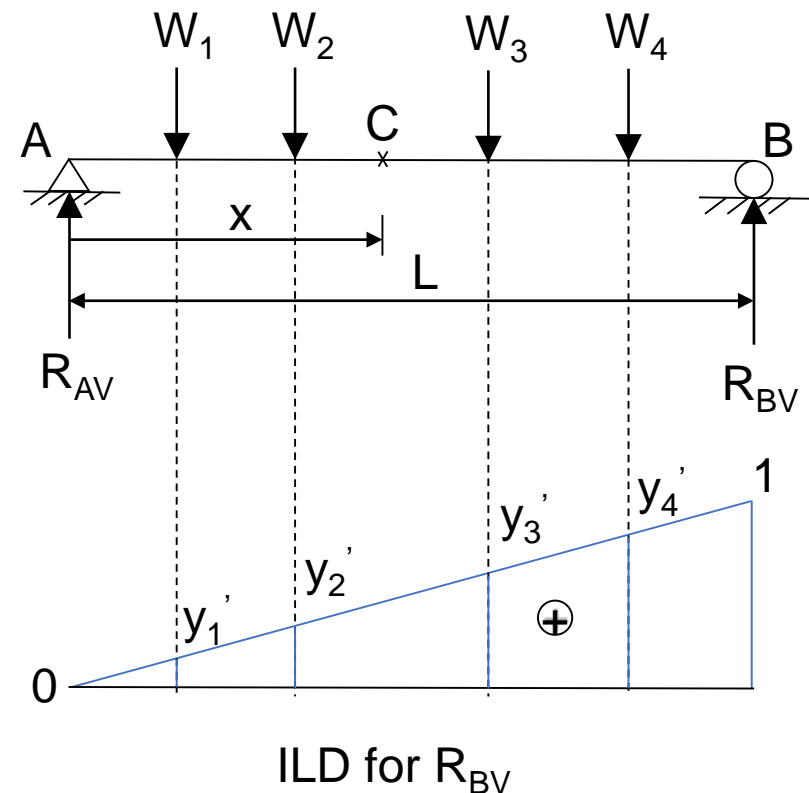
### Use of ILD (Point loads)

We have,  
ILD for  $R_{BV}$  for simply supported beam as shown in the adjacent figure.

Let  $y_1'$ ,  $y_2'$ ,  $y_3'$ , and  $y_4'$  be ordinates of ILD for  $R_{BV}$  at load points  $W_1$ ,  $W_2$ ,  $W_3$ , and  $W_4$ , respectively.

Then,  
 $R_{BV}$  due to the given loadings  

$$= W_1 * y_1' + W_2 * y_2' + W_3 * y_3' + W_4 * y_4'$$



## 5.9 Determination of Reactions, BM, and SF from ILDs for Different Loadings

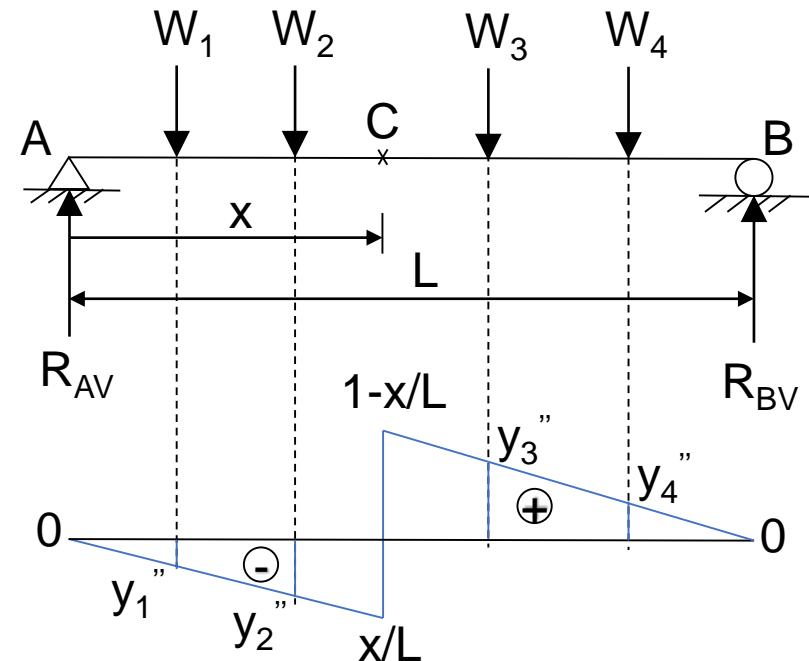
### Use of ILD (Point loads)

We have,  
ILD for SF at C for simply supported beam as shown in the adjacent figure.

Let  $y_1''$ ,  $y_2''$ ,  $y_3''$ , and  $y_4''$  be ordinates of ILD for SF at C at load points  $W_1$ ,  $W_2$ ,  $W_3$ , and  $W_4$ , respectively.

Then,  
SF at C due to the given loadings  

$$= W_1 * -y_1'' + W_2 * -y_2'' + W_3 * y_3'' + W_4 * y_4''$$



ILD for SF at C

## 5.9 Determination of Reactions, BM, and SF from ILDs for Different Loadings

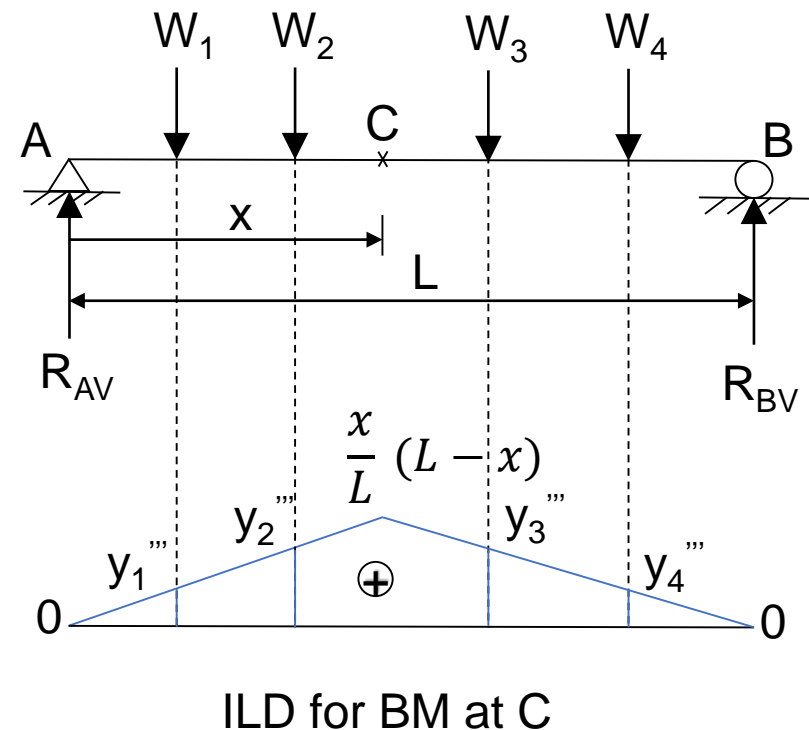
### Use of ILD (Point loads)

We have,  
ILD for BM at C for simply supported beam as shown in the adjacent figure.

Let  $y_1''''$ ,  $y_2''''$ ,  $y_3''''$ , and  $y_4''''$  be ordinates of ILD for BM at C at load points  $W_1$ ,  $W_2$ ,  $W_3$ , and  $W_4$ , respectively.

Then,  
BM at C due to the given loadings  

$$= W_1 * y_1'''' + W_2 * y_2'''' + W_3 * y_3'''' + W_4 * y_4''''$$



## 5.9 Determination of Reactions, BM, and SF from ILDs for Different Loadings

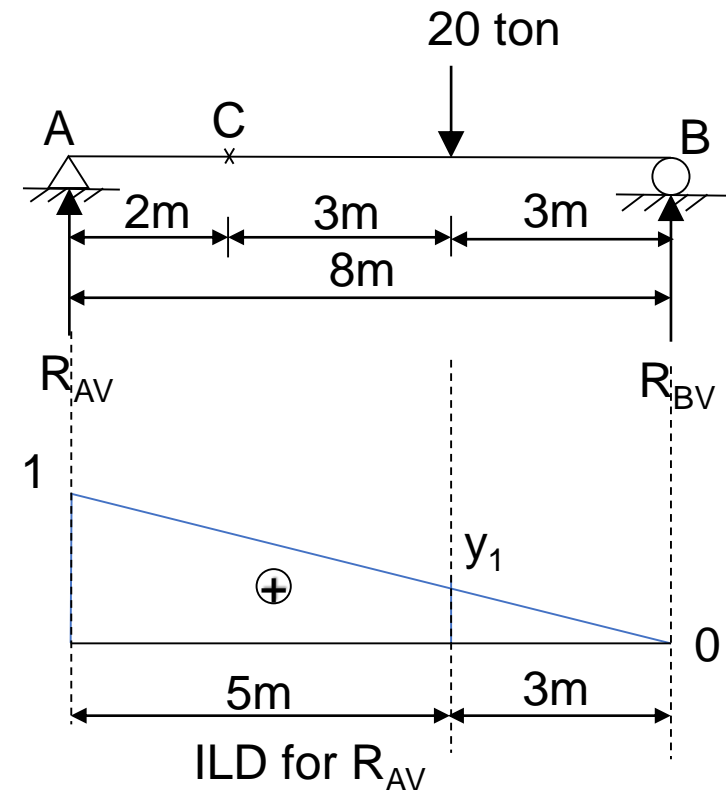
**Numerical #1.** Find the reaction at the supports, SF and BM at C of the given beam, using ILD.

We have,  
ILD for  $R_{AV}$  for simply supported beam AB as shown in the adjacent figure.

Now,  
Using similar triangles,

$$\frac{1}{5+3} = \frac{y_1}{3}$$

$$\text{Or, } y_1 = \frac{3}{8}$$



## 5.9 Determination of Reactions, BM, and SF from ILDs for Different Loadings

**Numerical #1.** Find the reaction at the supports, SF and BM at C of the given beam, using ILD.

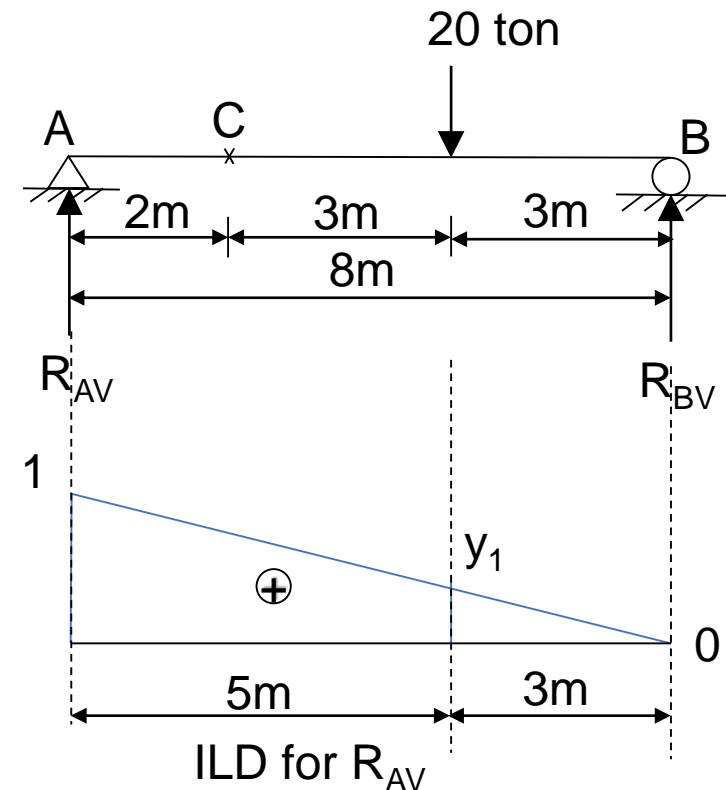
We have,

$$y_1 = \frac{3}{8}$$

Then,

$$R_{AV} = 20 * y_1 = 20 * \frac{3}{8} = \frac{15}{2} = 7.5 \text{ ton}$$

Ans.



## 5.9 Determination of Reactions, BM, and SF from ILDs for Different Loadings

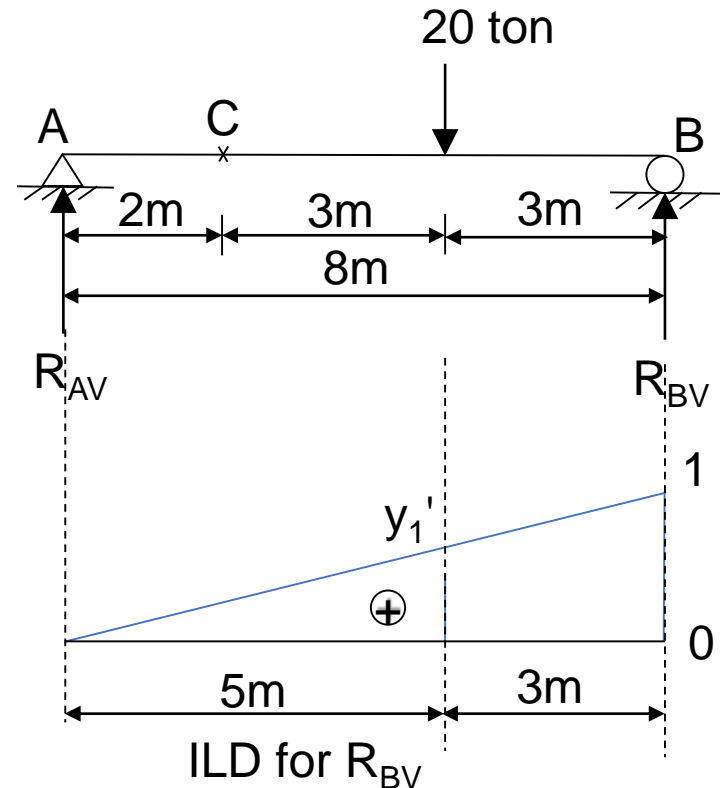
**Numerical #1.** Find the reaction at the supports, SF and BM at C of the given beam, using ILD.

We have,  
ILD for  $R_{BV}$  for simply supported beam AB as shown in the adjacent figure.

Now,  
Using similar triangles,

$$\frac{1}{5+3} = \frac{y_1'}{5}$$

$$\text{Or, } y_1' = \frac{5}{8}$$



## 5.9 Determination of Reactions, BM, and SF from ILDs for Different Loadings

**Numerical #1.** Find the reaction at the supports, SF and BM at C of the given beam, using ILD.

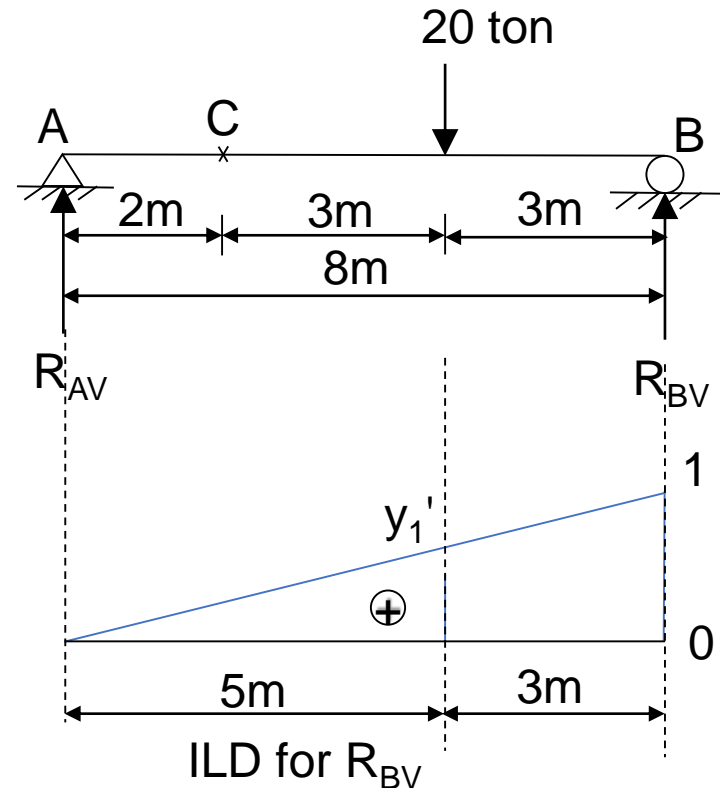
We have,

$$y_1' = \frac{5}{8}$$

Then,

$$R_{BV} = 20 * y_1' = 20 * \frac{5}{8} = \frac{25}{2} = 12.5 \text{ ton}$$

Ans.



## 5.9 Determination of Reactions, BM, and SF from ILDs for Different Loadings

**Numerical #1.** Find the reaction at the supports, SF and BM at C of the given beam, using ILD.

We have,

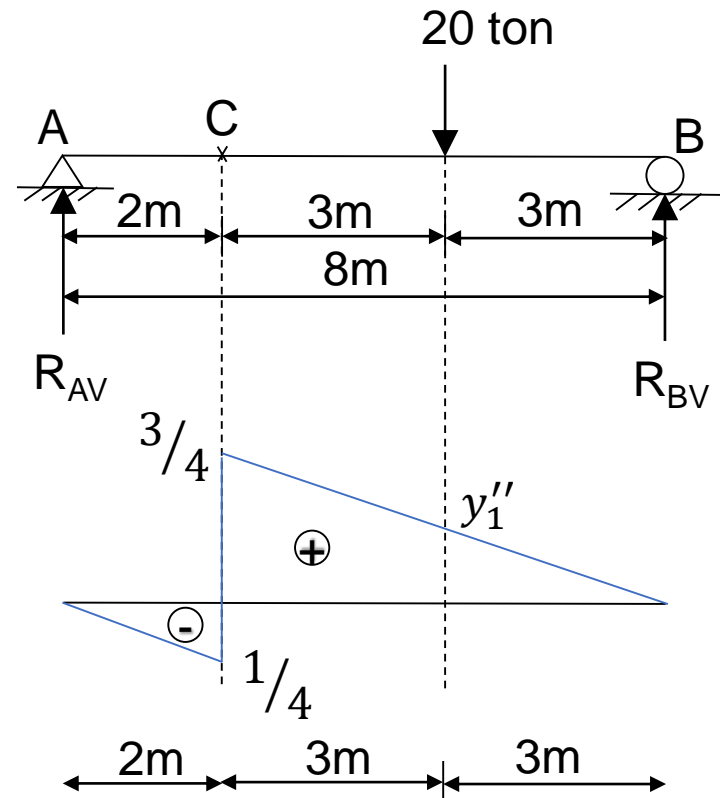
ILD for **SF at C** for simply supported beam AB as shown in the adjacent figure, where

$$\frac{x}{L} = \frac{2}{8} = \frac{1}{4} \text{ and } 1 - \frac{x}{L} = 1 - \frac{1}{4} = \frac{3}{4}$$

Now,

Using similar triangles,

$$\frac{3/4}{3+3} = \frac{y_1''}{3} \quad \text{Or, } y_1'' = \frac{3}{8}$$



ILD for SF at C

## 5.9 Determination of Reactions, BM, and SF from ILDs for Different Loadings

**Numerical #1.** Find the reaction at the supports, SF and BM at C of the given beam, using ILD.

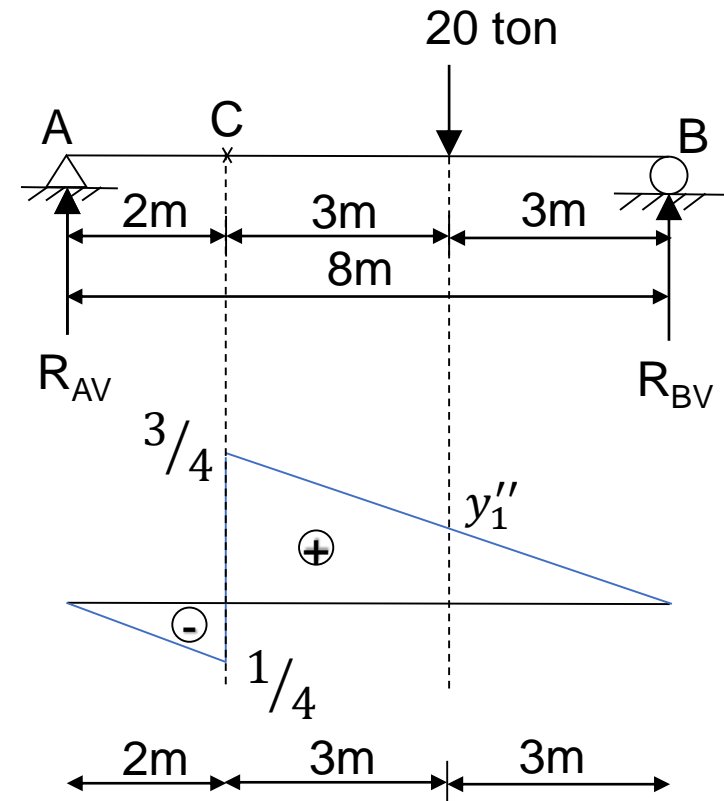
We have,

$$y_1'' = \frac{3}{8}$$

Then,

$$SF \text{ at } C = 20 * y_1'' = 20 * \frac{3}{8} = \frac{15}{2} = 7.5 \text{ ton}$$

Ans.



ILD for SF at C

## 5.9 Determination of Reactions, BM, and SF from ILDs for Different Loadings

**Numerical #1.** Find the reaction at the supports, SF and BM at C of the given beam, using ILD.

We have,

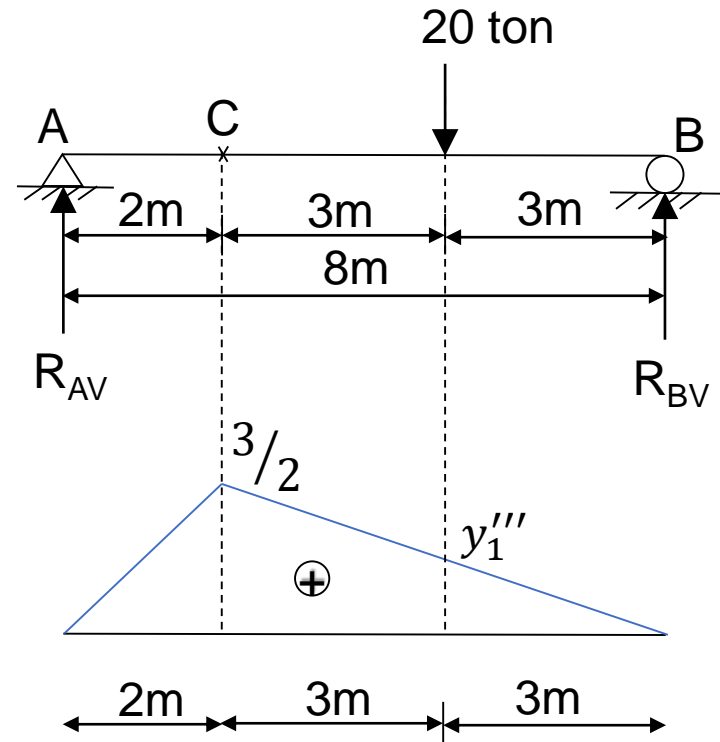
ILD for **BM at C** for simply supported beam AB as shown in the adjacent figure, where

$$\frac{x}{L} (L - x) = \frac{2}{8} (8 - 2) = \frac{1}{4} * 6 = \frac{3}{2}$$

Now,

Using similar triangles,

$$\frac{3/2}{3 + 3} = \frac{y_1'''}{3} \quad \text{Or, } y_1''' = \frac{3}{4}$$



ILD for BM at C

## 5.9 Determination of Reactions, BM, and SF from ILDs for Different Loadings

**Numerical #1.** Find the reaction at the supports, SF and BM at C of the given beam, using ILD.

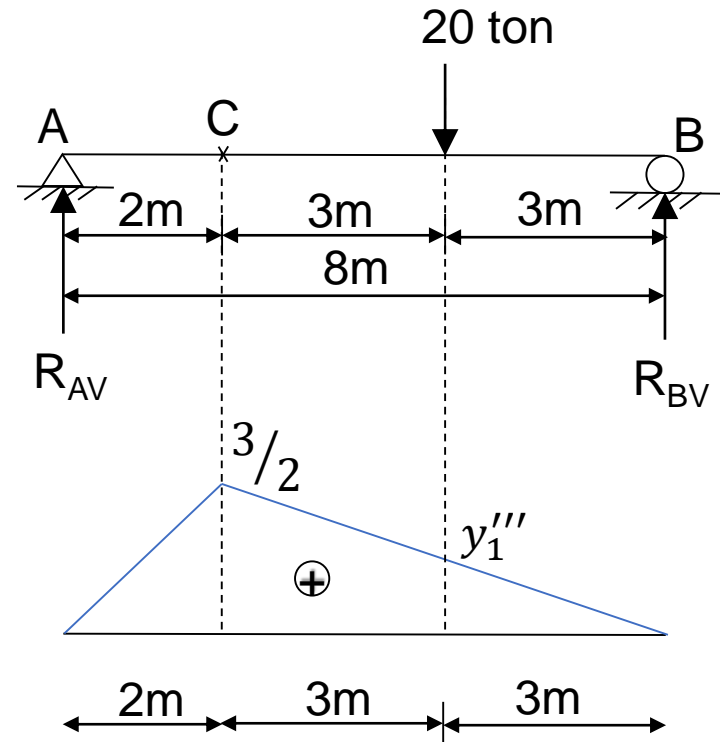
We have,

$$y_1''' = \frac{3}{4}$$

Then,

$$\mathbf{BM \text{ at } C = 20 * y_1''' = 20 * \frac{3}{4} = 15 \text{ ton}}$$

Ans.



ILD for BM at C

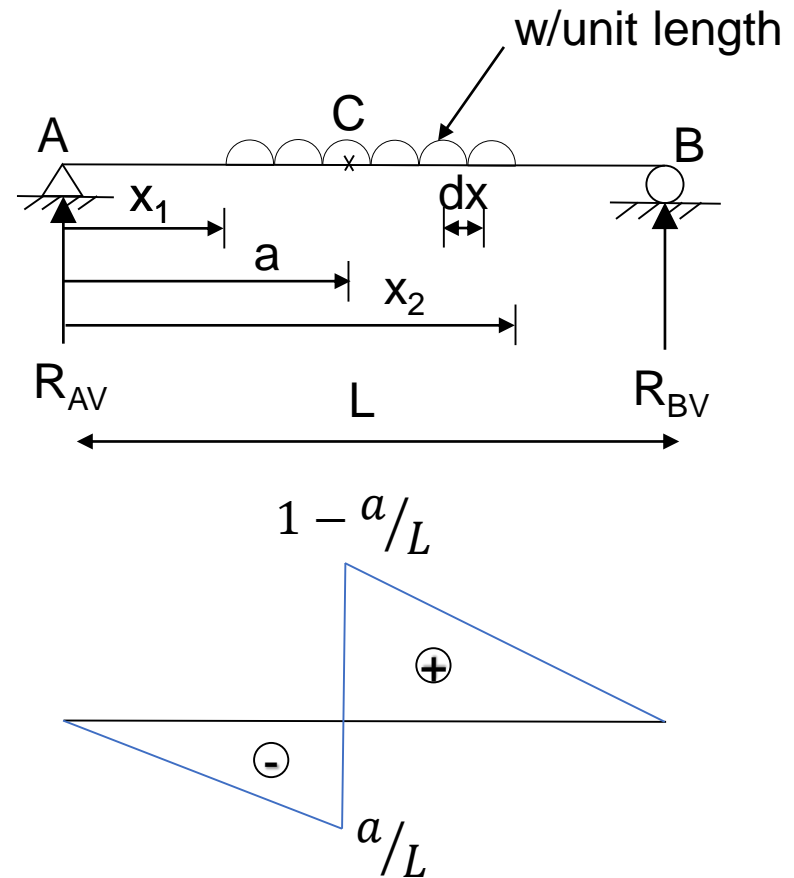
## 5.9 Determination of Reactions, BM, and SF from ILDs for Different Loadings

### Use of ILD (Uniformly Distributed Load)

Let us consider a UDL  $w$ /unit length acting at a distance from  $x_1$  to  $x_2$  from support A on the simply supported beam AB of length  $L$ .

We need to compute the SF and BM at section C at a distance  $a$  from support A.

Then, we have,  
ILD for SF at C for a simply supported beam is:



ILD for SF at C

## 5.9 Determination of Reactions, BM, and SF from ILDs for Different Loadings

### Use of ILD (Uniformly Distributed Load)

Here, for SF at C due to elemental load,  $w \cdot dx = (w \cdot dx) \cdot y$ ,

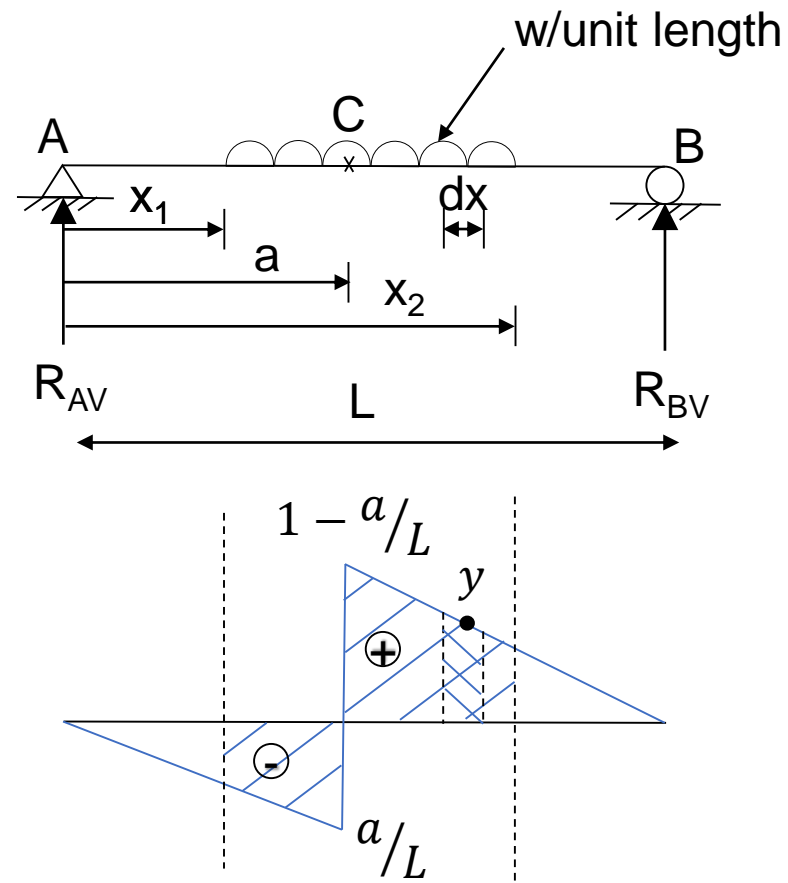
Where,  $y$  is the ordinate of ILD for SF at C.

Then,

SF at C due to UDL from  $x_1$  to  $x_2$

$$= \int_{x_1}^{x_2} w \cdot y \, dx = w \int_{x_1}^{x_2} y \, dx$$

=  $w$  \* area of shaded portion  
under the load of ILD for SF at C



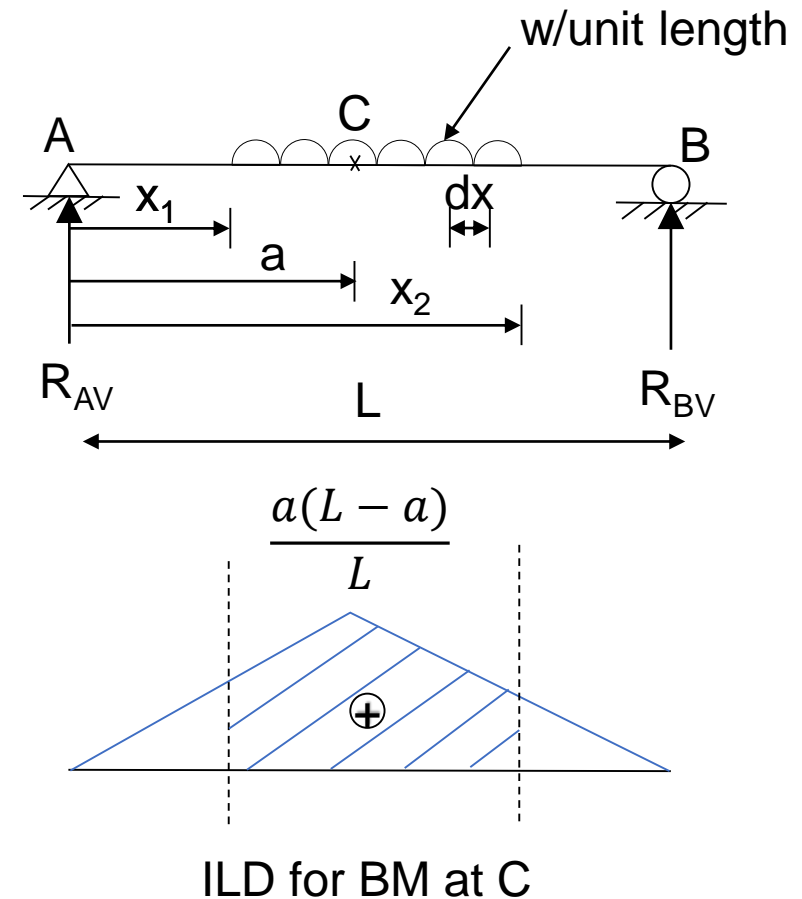
ILD for SF at C

## 5.9 Determination of Reactions, BM, and SF from ILDs for Different Loadings

### Use of ILD (Uniformly Distributed Load)

We have,  
ILD for BM at C for a simply supported beam is:

Similarly,  
BM at C due to UDL  
=  $w \cdot \text{area of shaded portion under the load of ILD for BM at C}$



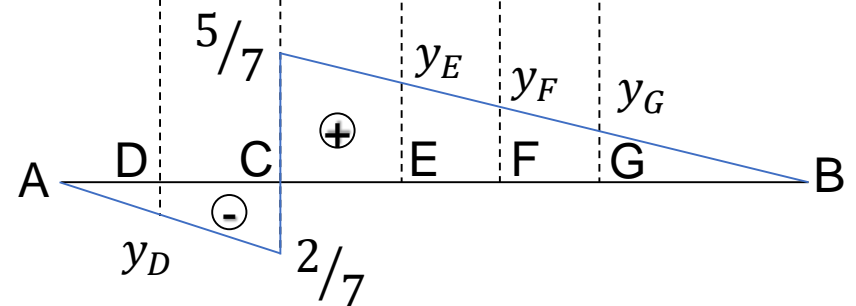
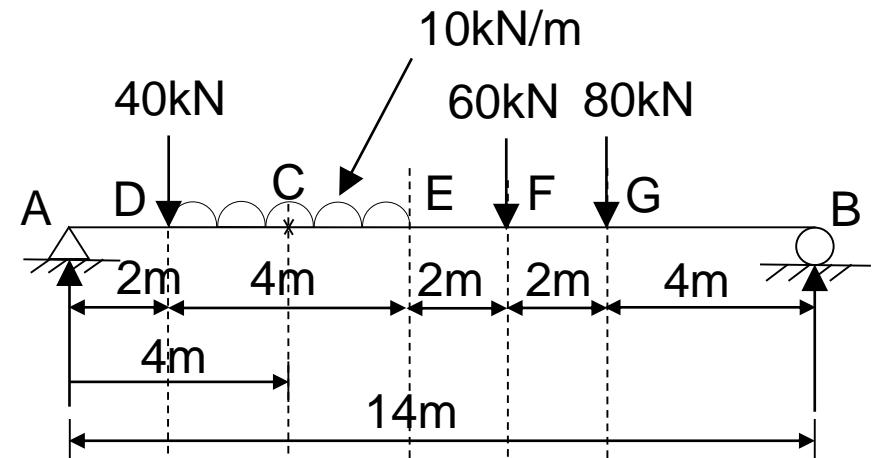
## 5.9 Determination of Reactions, BM, and SF from ILDs for Different Loadings

**Numerical #2.** Using ILD, determine the SF and BM at section C in the given simply supported beam.

We have,  
ILD for SF at C for a simply supported beam, where  
 $\frac{x}{L} = \frac{4}{14} = \frac{2}{7}$  and  $1 - \frac{2}{7} = \frac{5}{7}$

Now, using similar triangles, the ordinate at load point D is:

$$\frac{2/7}{4} = \frac{y_D}{2} \quad \text{Or, } y_D = \frac{1}{7}$$



ILD for SF at C

## 5.9 Determination of Reactions, BM, and SF from ILDs for Different Loadings

**Numerical #2.** Using ILD, determine the SF and BM at section C in the given simply supported beam.

The ordinate at load point E is:

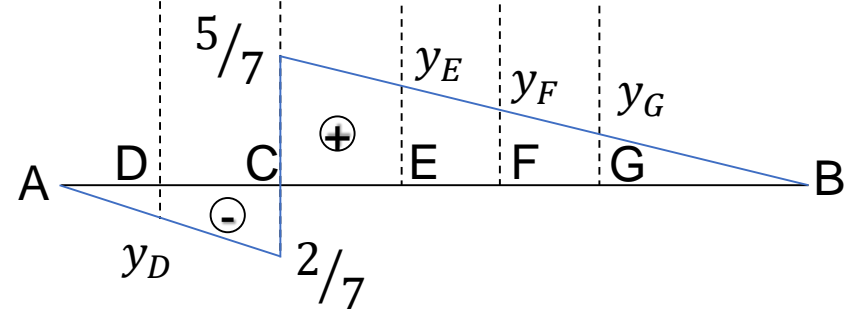
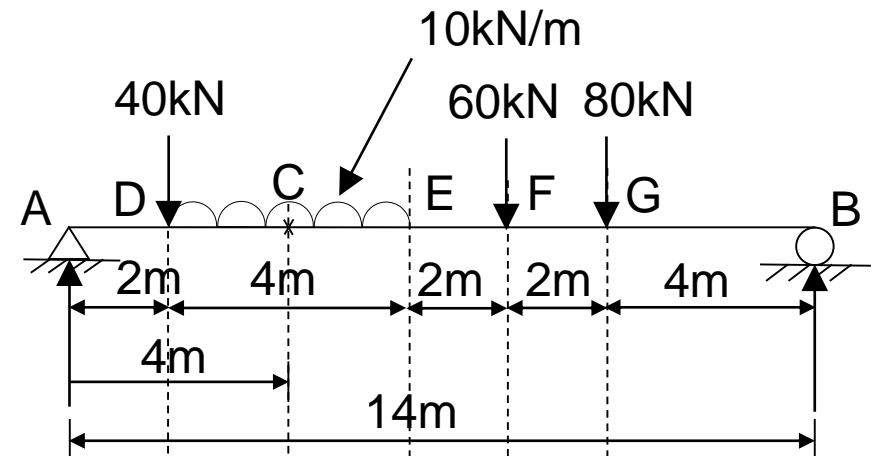
$$\frac{5/7}{10} = \frac{y_E}{8} \quad \text{Or, } y_E = \frac{4}{7}$$

The ordinate at load point F is:

$$\frac{5/7}{10} = \frac{y_F}{6} \quad \text{Or, } y_F = \frac{3}{7}$$

The ordinate at load point G is:

$$\frac{5/7}{10} = \frac{y_G}{4} \quad \text{Or, } y_G = \frac{2}{7}$$



ILD for SF at C

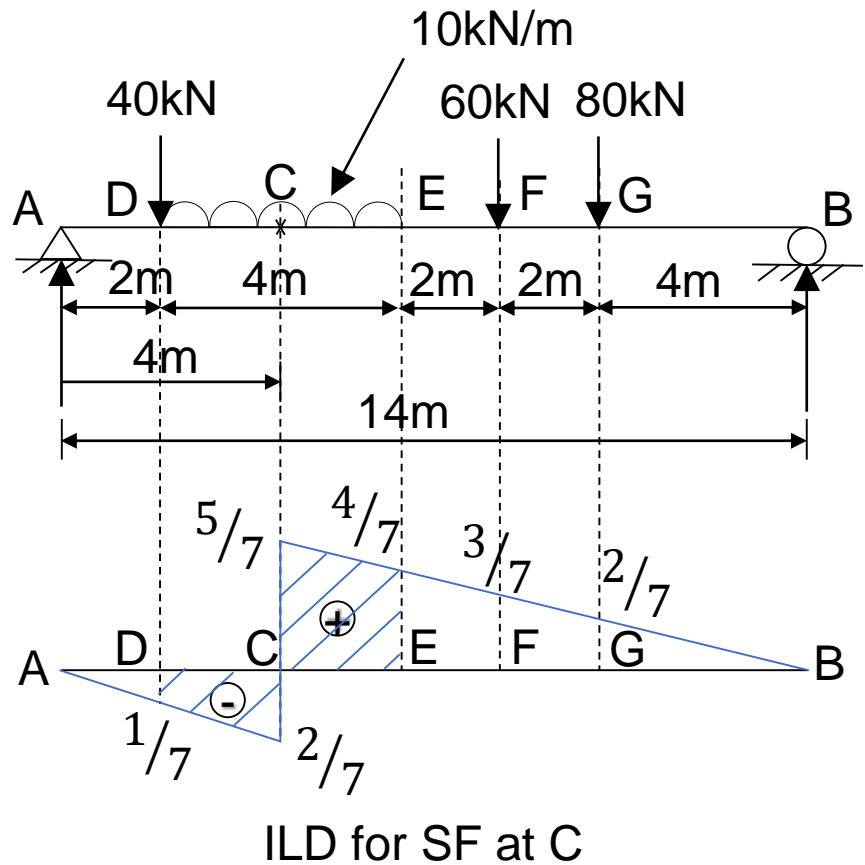
# 5.9 Determination of Reactions, BM, and SF from ILDs for Different Loadings

**Numerical #2.** Using ILD, determine the SF and BM at section C in the given simply supported beam.

We get,

the ordinates at load points D, E, F, and G in ILD for SF at C as  $1/7$ ,  $4/7$ ,  $3/7$ , and  $2/7$ , respectively.

Then,  
 SF at C =  $40 \cdot y_D - 10 \cdot (\text{trapezoidal shaded area under UDL between D and C}) + 10 \cdot (\text{trapezoidal shaded area under UDL between C and E}) + 60 \cdot y_F + 80 \cdot y_G$



Source: Bhavikatti, S. S. (2011). *Structural Analysis – I* (4<sup>th</sup> ed.). New Delhi: Vikas Publishing House.

## 5.9 Determination of Reactions, BM, and SF from ILDs for Different Loadings

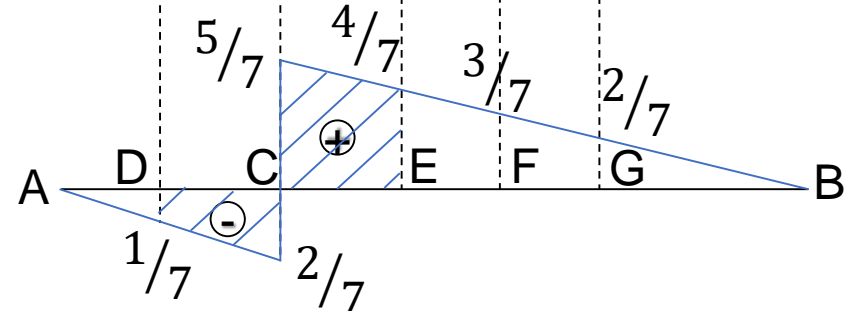
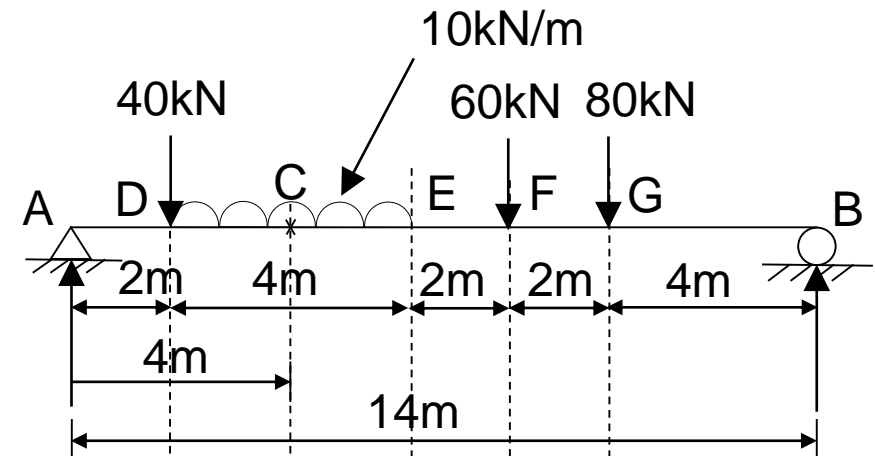
**Numerical #2.** Using ILD, determine the SF and BM at section C in the given simply supported beam.

Then,

**SF at C**

$$\begin{aligned}
 &= 40 \times -\frac{1}{7} - 10 \times \frac{1}{2} \times \left(\frac{1}{7} + \frac{2}{7}\right) \times 2 + 10 \times \frac{1}{2} \times \left(\frac{5}{7} + \frac{4}{7}\right) \times 2 + 60 \times \frac{3}{7} + 80 \times \frac{2}{7} \\
 &= \mathbf{51.43 \text{ kN}}
 \end{aligned}$$

Ans.



ILD for SF at C

## 5.9 Determination of Reactions, BM, and SF from ILDs for Different Loadings

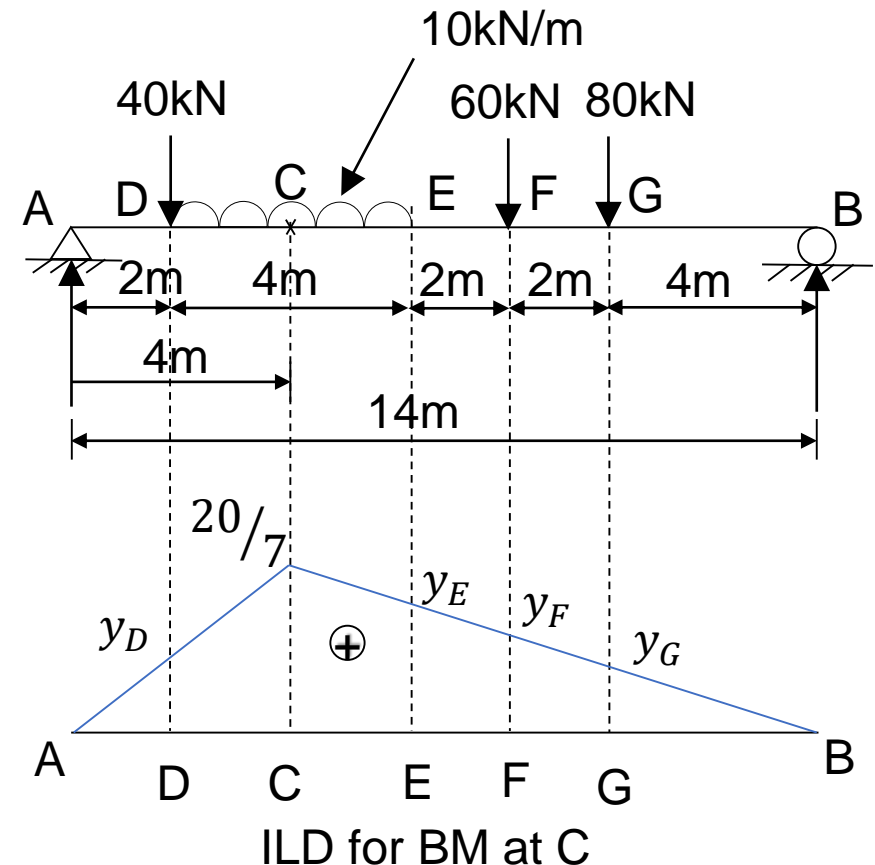
**Numerical #2.** Using ILD, determine the SF and BM at section C in the given simply supported beam.

We have,  
ILD for BM at C for a simply supported beam, where

$$\frac{x(L-x)}{L} = \frac{4(14-4)}{14} = \frac{20}{7}$$

Now, using similar triangles, the ordinate at load point D is:

$$\frac{20/7}{4} = \frac{y_D}{2} \quad \text{Or, } y_D = \frac{10}{7}$$



## 5.9 Determination of Reactions, BM, and SF from ILDs for Different Loadings

**Numerical #2.** Using ILD, determine the SF and BM at section C in the given simply supported beam.

The ordinate at load point E is:

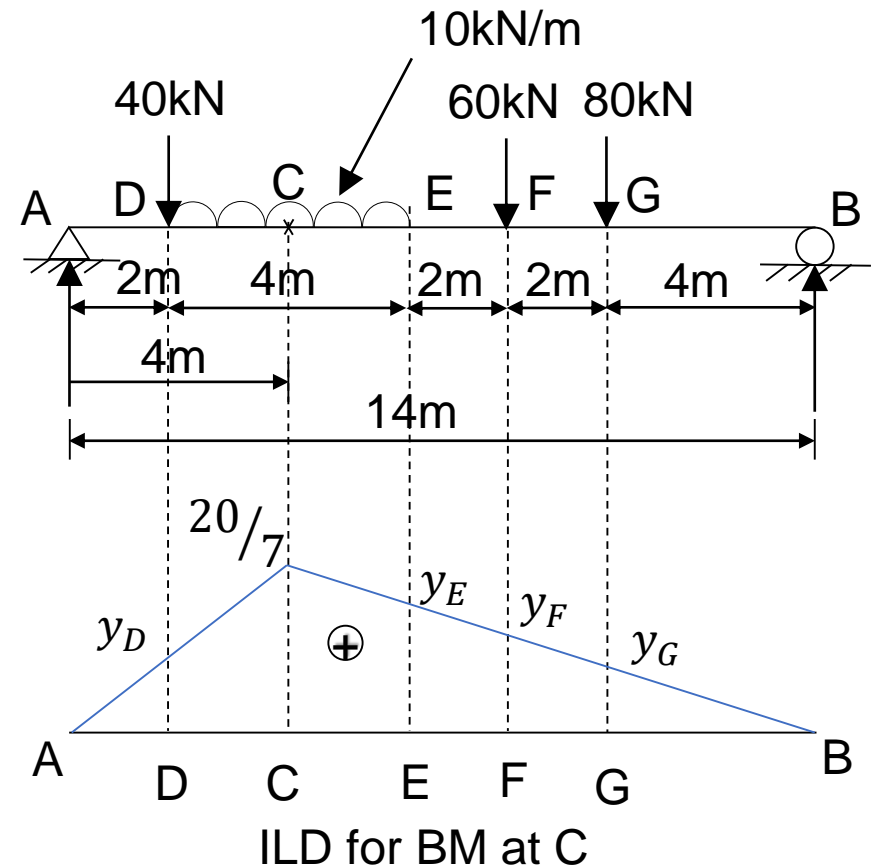
$$\frac{20/7}{10} = \frac{y_E}{8} \quad \text{Or, } y_E = \frac{16}{7}$$

The ordinate at load point F is:

$$\frac{20/7}{10} = \frac{y_F}{6} \quad \text{Or, } y_F = \frac{12}{7}$$

The ordinate at load point G is:

$$\frac{20/7}{10} = \frac{y_G}{4} \quad \text{Or, } y_G = \frac{8}{7}$$



## 5.9 Determination of Reactions, BM, and SF from ILDs for Different Loadings

**Numerical #2.** Using ILD, determine the SF and BM at section C in the given simply supported beam.

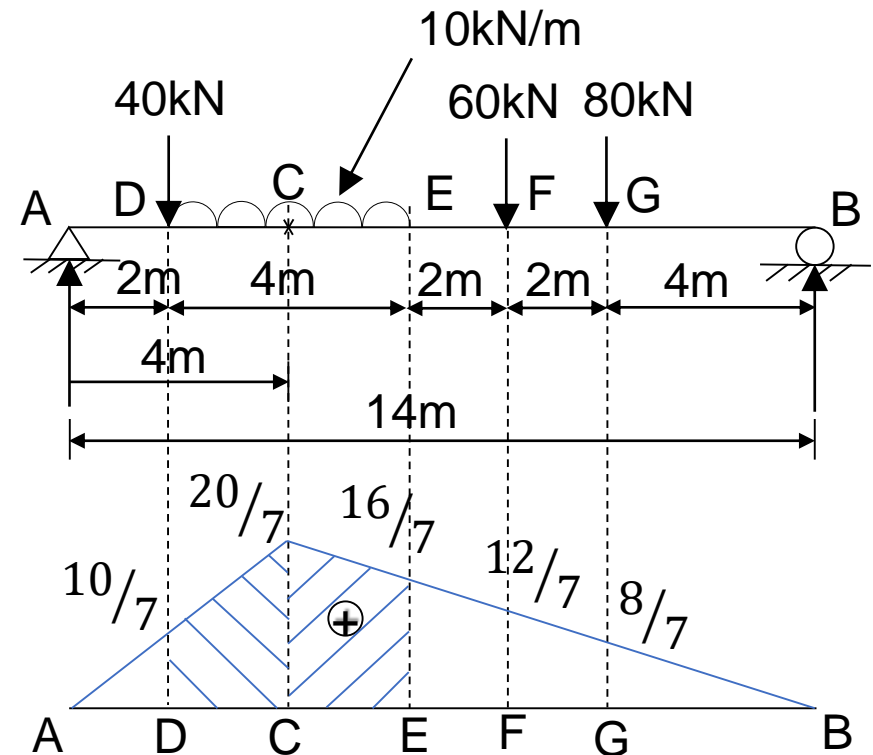
We get,

the ordinates at load points D, E, F, and G in ILD for BM at C as  $10/7$ ,  $16/7$ ,  $12/7$ , and  $8/7$ , respectively.

Then,

BM at C

$$= 40 * y_D + 10 * (\text{trapezoidal shaded area under UDL between D and C}) + 10 * (\text{trapezoidal shaded area under UDL between C and E}) + 60 * y_F + 80 * y_G$$



ILD for BM at C

# 5.9 Determination of Reactions, BM, and SF from ILDs for Different Loadings

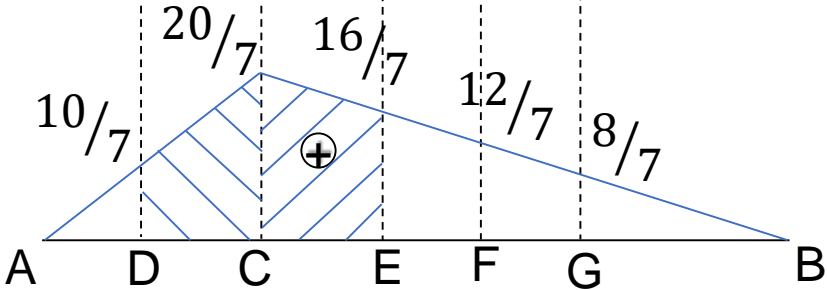
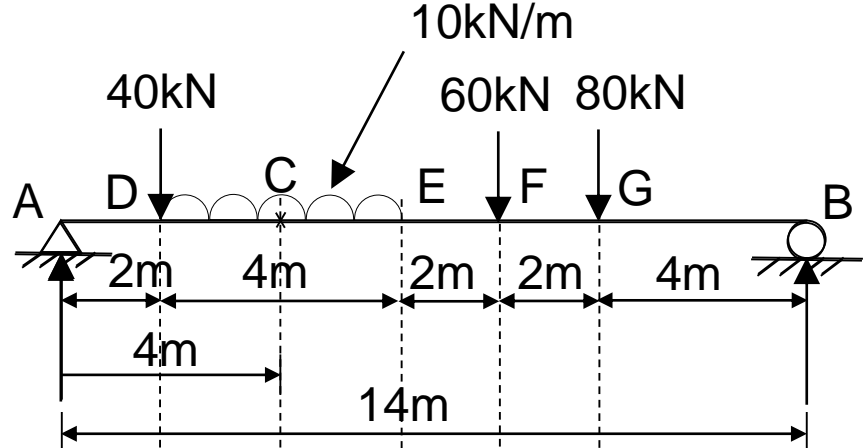
**Numerical #2.** Using ILD, determine the SF and BM at section C in the given simply supported beam.

Then,

**BM at C**

$$\begin{aligned}
 &= 40 * 10/7 + 10 * \frac{1}{2} \\
 & * (10/7 + 20/7) * 2 + 10 * \frac{1}{2} \\
 & * (20/7 + 16/7) * 2 + 60 * 12/7 + 80 * 8/7 \\
 &= \mathbf{345.71 \text{ kN-m.}}
 \end{aligned}$$

Ans.



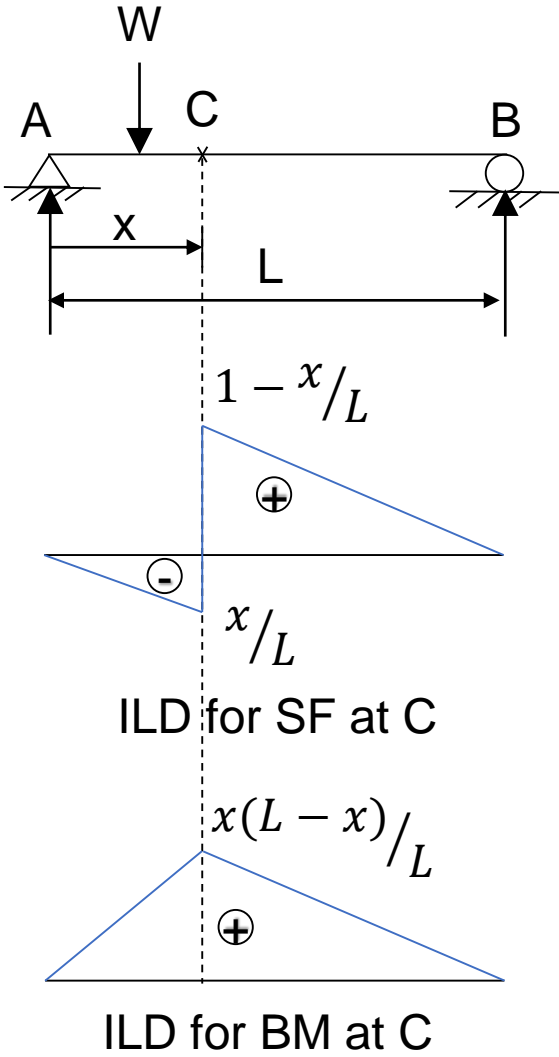
ILD for BM at C

# 5.10 Most critical position of a load on a beam span

**[A] Single point load**  
**(i) Maximum SF and BM**

Let  $W$  be the moving load and the values of maximum SF and BM is required at section C at a distance  $x$  from support A of the simply supported beam AB of span  $L$ .

|                 |                     | Location                           |
|-----------------|---------------------|------------------------------------|
| Max -ve SF at C | $W \cdot x/L$       | When $W$ is just to the left of C  |
| Max +ve SF at C | $W \cdot (1 - x/L)$ | When $W$ is just to the right of C |
| Max BM at C     | $W \cdot x(L-x)/L$  | When $W$ is on C                   |



Source: Bhavikatti, S. S. (2011). *Structural Analysis – I* (4<sup>th</sup> ed.). New Delhi: Vikas Publishing House.

## 5.10 Most critical position of a load on a beam span

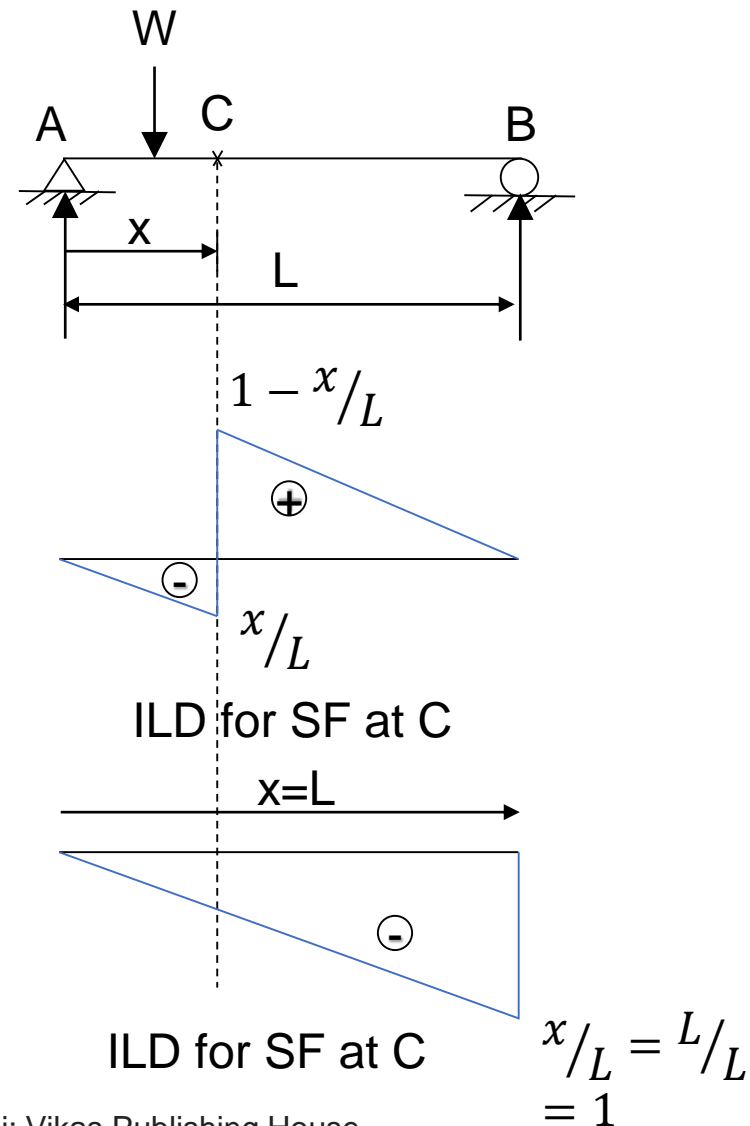
**[A] Single point load**  
**(ii) Absolute Maximum values**  
**anywhere in the beam**

For this, the ordinate of ILD should be maximum.

### ILD for SF at C

Negative SF ordinate is maximum when  $x=L$  and the value is equal to 1.

$\therefore$  Absolute maximum negative SF =  $W \cdot 1 = W$  and it occurs when  $W$  is at  $x=L$ , i.e. at B.



# 5.10 Most critical position of a load on a beam span

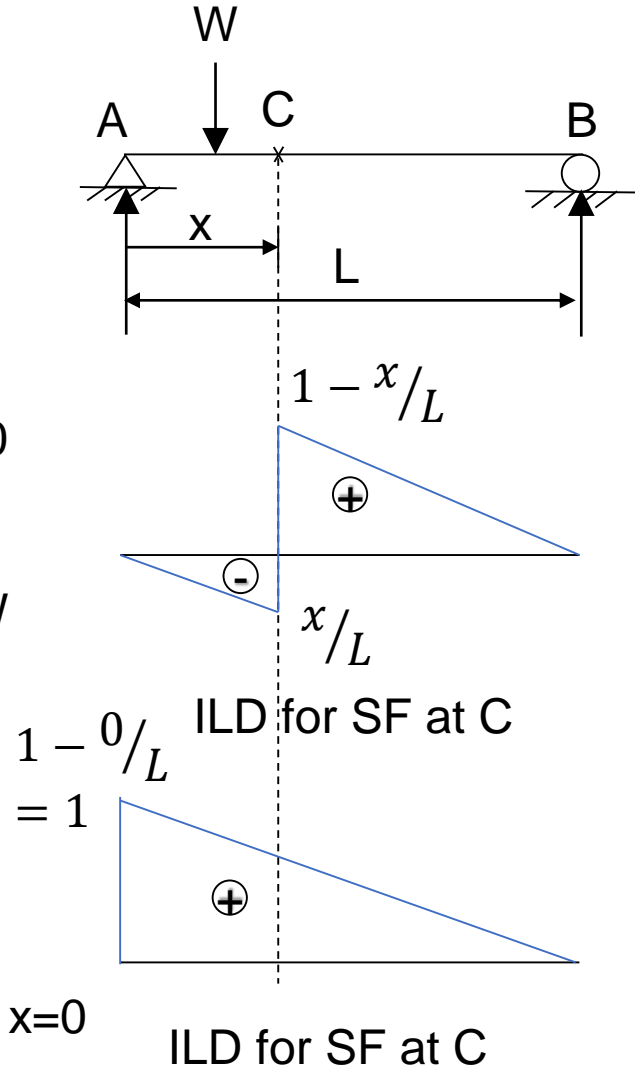
**[A] Single point load**  
**(ii) Absolute Maximum values**  
**anywhere in the beam**

**ILD for SF at C**

Positive SF ordinate is maximum when  $x=0$  and the value is equal to 1.

$\therefore$  Absolute maximum positive SF =  $W \cdot 1 = W$  and it occurs when  $W$  is at  $x=0$ , i.e. at A.

$\therefore$  Absolute maximum SF =  $W$



## 5.10 Most critical position of a load on a beam span

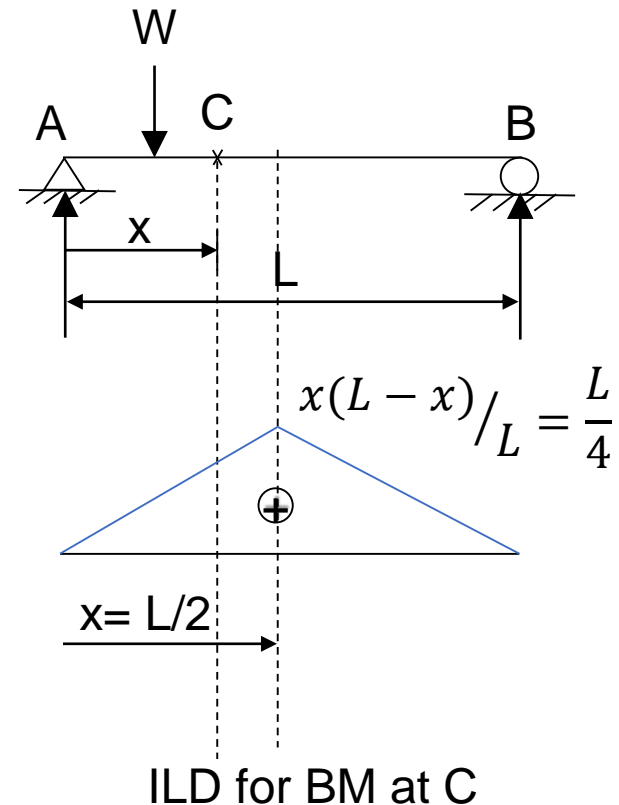
**[A] Single point load**  
**(ii) Absolute Maximum values**  
**anywhere in the beam**

### ILD for BM at C

BM ordinate is maximum when  $x=L/2$ , i.e. when the load  $W$  is at mid-span, which is equal to:

$$\frac{L}{2} * \left(L - \frac{L}{2}\right) / L = \frac{L}{4}$$

∴ Absolute maximum BM =  $W * \frac{L}{4} = \frac{WL}{4}$  and it occurs at mid-span.



## 5.10 Most critical position of a load on a beam span

**[B] UDL longer than the span ( $d > L$ )**  
**(i) Maximum SF and BM at given section**

Let a UDL of intensity  $w$  move from left to right across a beam AB

**ILD for SF at C**

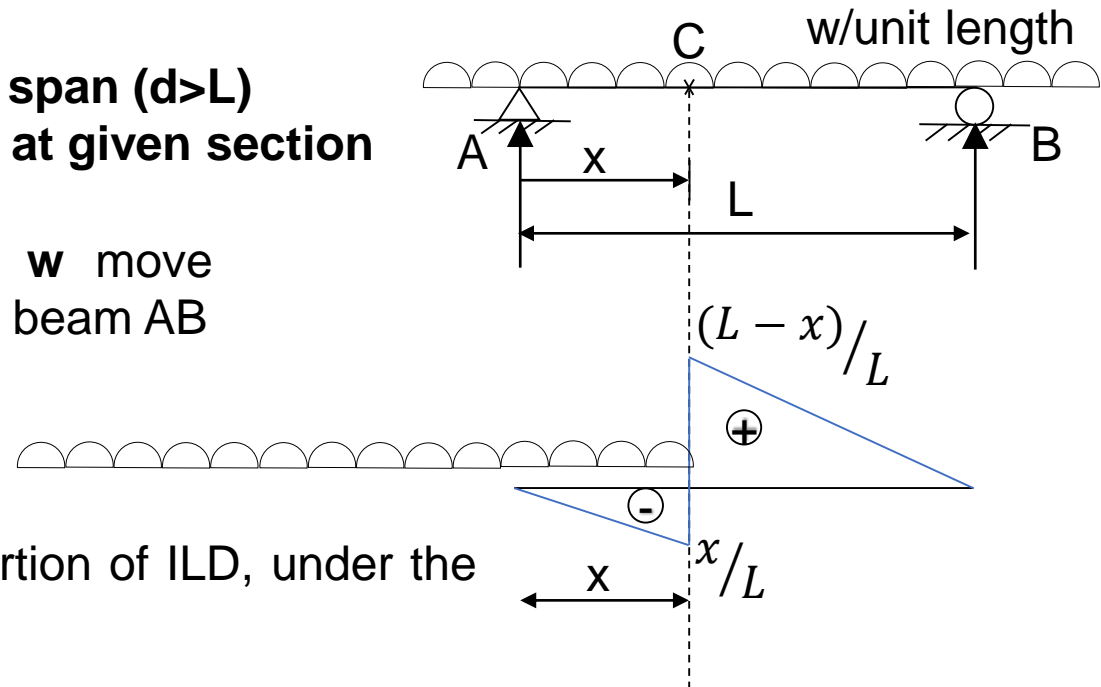
Maximum -ve SF

=  $w$  \* area of shaded portion of ILD, under the load

And, it occurs when UDL covers the portion AC only, as shown in the adjacent figure.

Then,

Maximum -ve SF at C =  $w * (\frac{1}{2} * x * x/L) = wx^2/2L$



ILD for SF at C

## 5.10 Most critical position of a load on a beam span

**[B] UDL longer than the span ( $d > L$ )**  
**(i) Maximum SF and BM at given section**

Let a UDL of intensity  $w$  move from left to right across a beam AB

**ILD for SF at C**

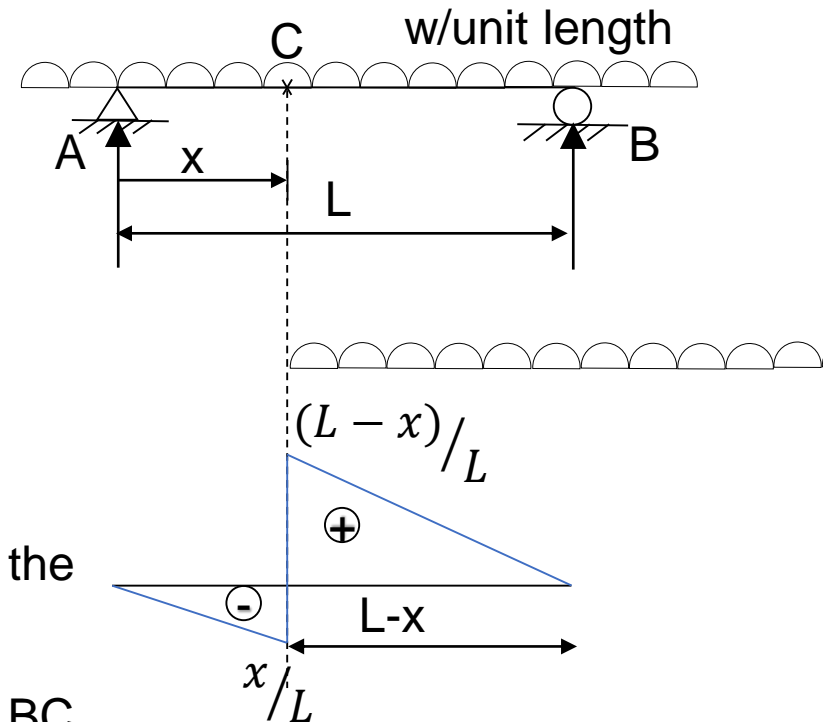
Maximum +ve SF

=  $w$  \* area of shaded portion of ILD, under the load

And, it occurs when UDL covers the portion BC only, as shown in the adjacent figure.

Then,

$$\text{Maximum +ve SF at C} = w * \left(\frac{1}{2} * (L-x) * (L-x)/L\right) = w(L-x)^2/2L$$



ILD for SF at C

## 5.10 Most critical position of a load on a beam span

**[B] UDL longer than the span ( $d > L$ )**  
**(i) Maximum SF and BM at given section**

Let a UDL of intensity  $w$  move from left to right across a beam AB

**ILD for BM at C**

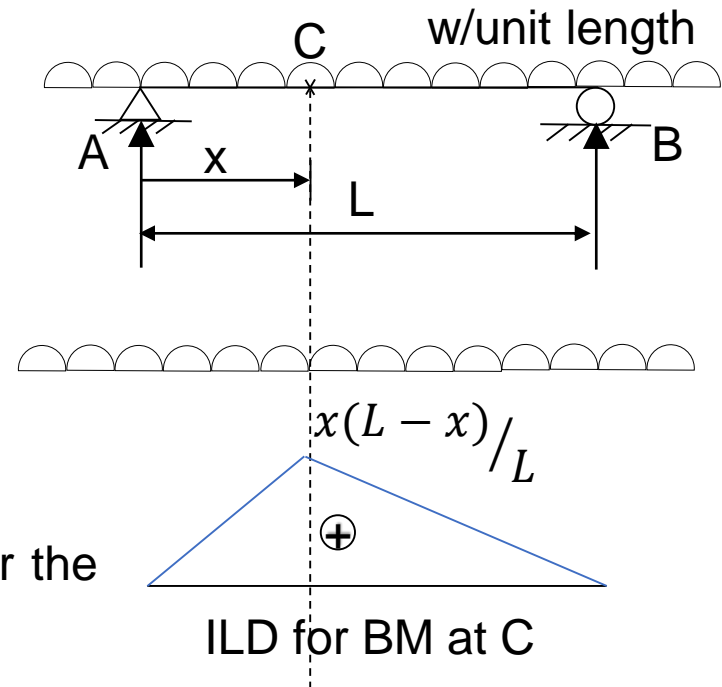
Maximum BM at C

=  $w$  \* area of shaded portion of ILD, under the load

And, it occurs when UDL covers the entire span of the beam, as shown in the adjacent figure.

Then,

$$\text{Maximum BM at C} = w * \left( \frac{1}{2} * L * \frac{x(L-x)}{L} \right) = wx(L-x)/2$$



## 5.10 Most critical position of a load on a beam span

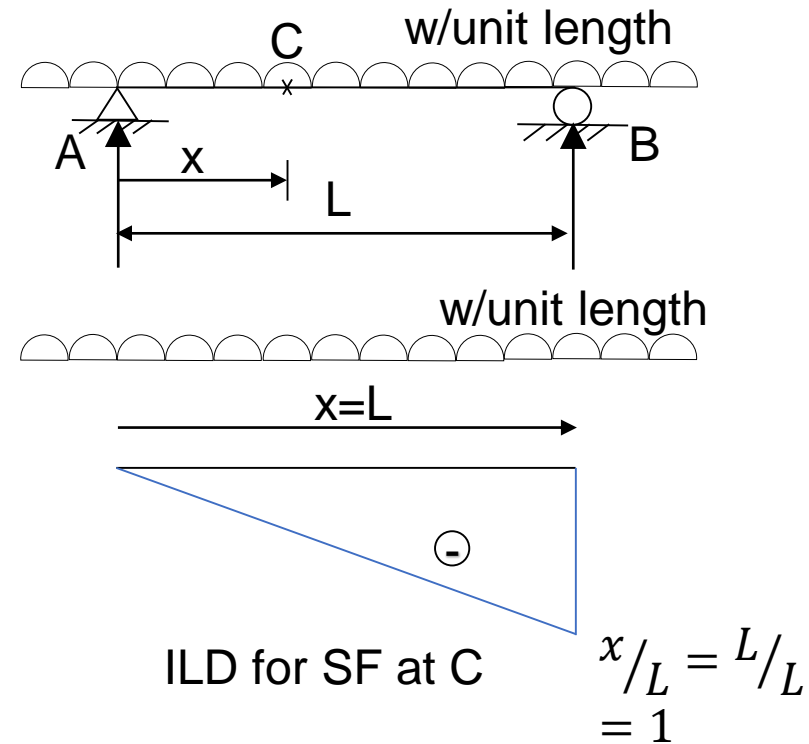
**[B] UDL longer than the span ( $d > L$ )**  
**(ii) Absolute Maximum values anywhere in the beam**

**ILD for SF at C**

Negative SF ordinate is maximum when  $x=L$  and the value is equal to 1.

$$\begin{aligned} \therefore \text{Absolute maximum negative SF} \\ &= w \cdot \frac{1}{2} \cdot L \cdot 1 \\ &= wL/2 \end{aligned}$$

And, it occurs when the UDL occupies the entire span of the beam.



## 5.10 Most critical position of a load on a beam span

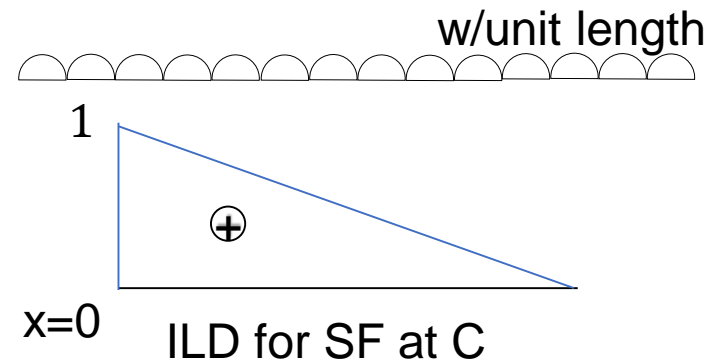
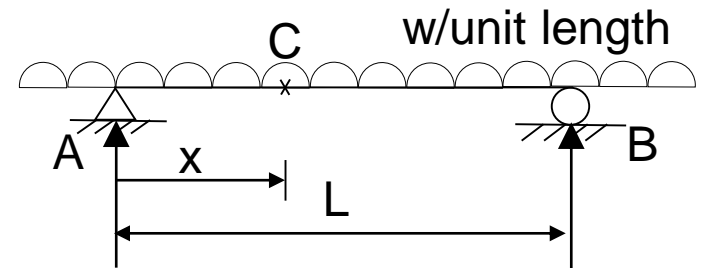
**[B] UDL longer than the span ( $d > L$ )**  
**(ii) Absolute Maximum values anywhere in the beam**

### ILD for SF at C

Positive SF ordinate is maximum when  $x=0$  and the value is equal to 1.

$$\begin{aligned} \therefore \text{Absolute maximum positive SF} \\ &= w \cdot 1/2 \cdot L \cdot 1 \\ &= wL/2 \end{aligned}$$

And, it occurs when the UDL occupies the entire span of the beam.



$$\therefore \text{Absolute maximum SF} = wL/2$$

## 5.10 Most critical position of a load on a beam span

**[B] UDL longer than the span ( $d > L$ )**  
**(ii) Absolute Maximum values**  
**anywhere in the beam**

**ILD for BM at C**

We have, Max BM at any section

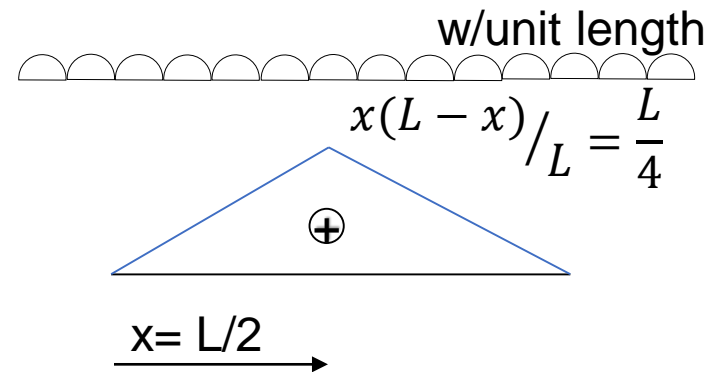
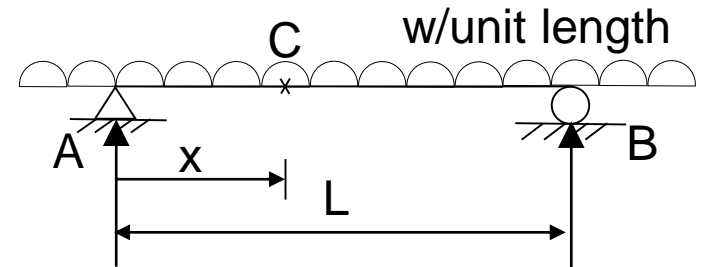
$$= \frac{w * x(L-x)}{2}$$

The value of which will be maximum when  $x=L/2$ , i.e. at mid-span.

$\therefore$  Absolute maximum BM

$$= \frac{w * \frac{L}{2} * (L - \frac{L}{2})}{2} = \frac{wL^2}{8}$$

And, it occurs when the UDL occupies the entire span of the beam.



ILD for BM at C

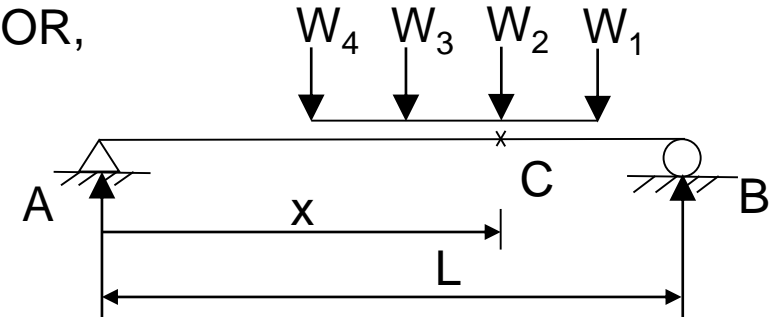
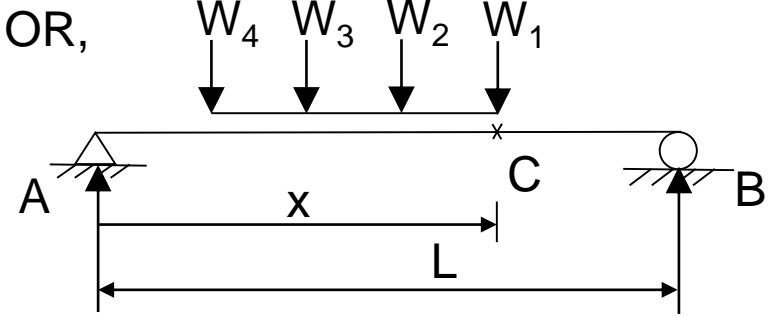
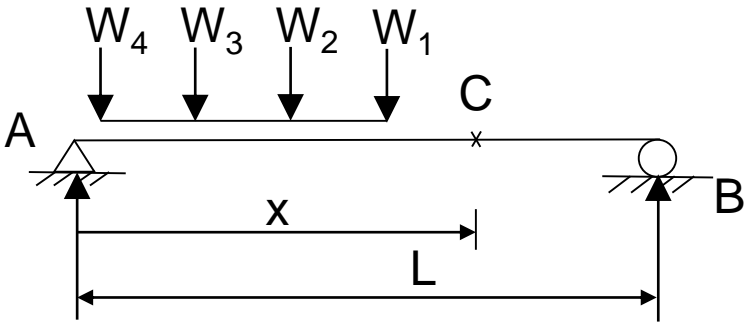
$$\therefore \text{Absolute maximum BM} = \frac{wL^2}{8}$$

# 5.10 Most critical position of a load on a beam span

**[C] A train of point loads**  
**(i) Maximum SF at a section**

The maximum negative or positive SF at a given section occurs when one of the loads is at the section itself, as shown in the adjacent figures.

From *trial and error*, we can determine which load should be placed over the section to get the maximum value.



Source: Bhavikatti, S. S. (2011). *Structural Analysis – I* (4<sup>th</sup> ed.). New Delhi: Vikas Publishing House.

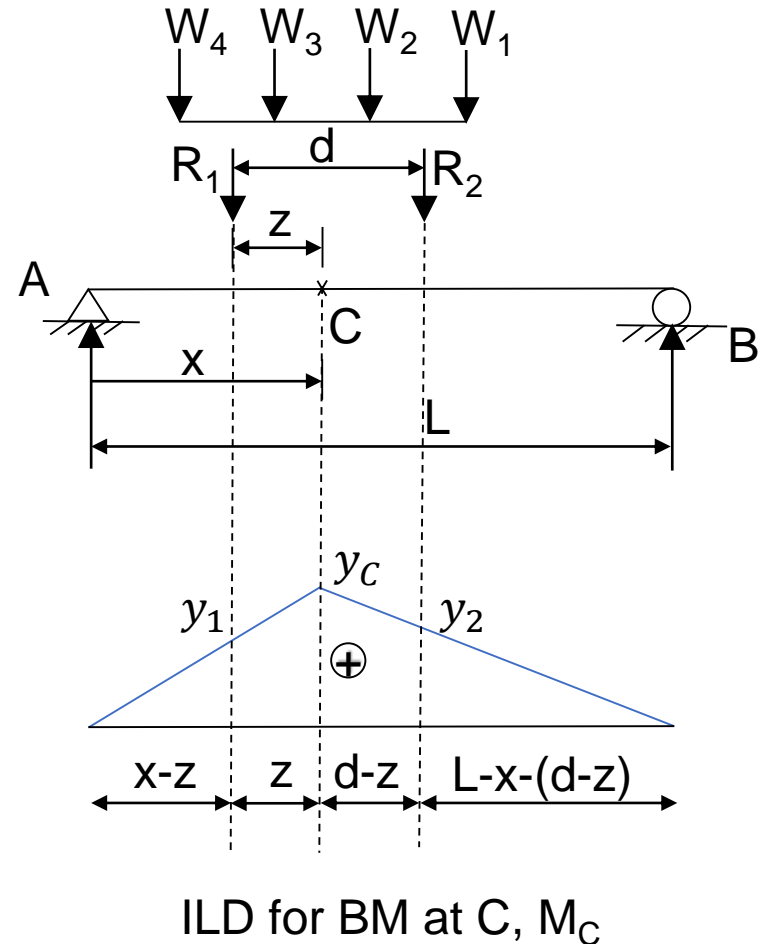
## 5.10 Most critical position of a load on a beam span

### [C] A train of point loads (ii) Maximum BM at a section

Let  $R_1$  and  $R_2$  be the resultant of loads on the left and the right of the section C, respectively.

Let the distance between  $R_1$  and  $R_2$  be  $d$ , and the distance of  $R_1$  from section C be  $z$ .

Let the ordinate of ILD for moment at C be  $y_1$  under  $R_1$  and  $y_2$  under  $R_2$ , and the maximum ordinate at C be  $y_c$ .



## 5.10 Most critical position of a load on a beam span

[C] A train of point loads  
(ii) Maximum BM at a section

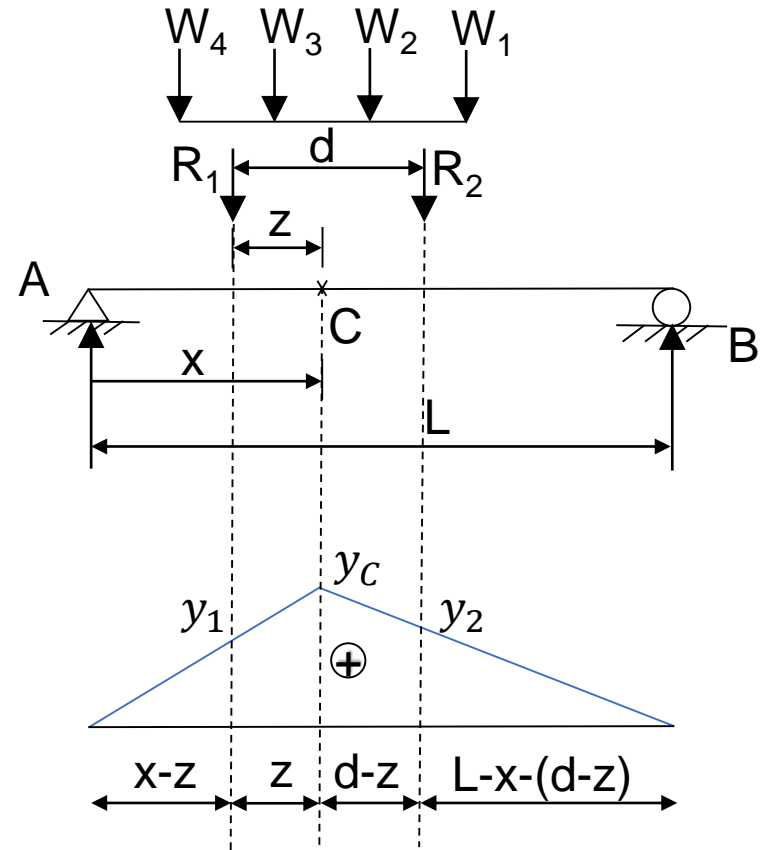
Then, using similar triangles,

$$\frac{y_C}{x} = \frac{y_1}{x-z} \quad \text{Or, } y_1 = \frac{x-z}{x} * y_C$$

And,

$$\frac{y_C}{L-x} = \frac{y_2}{L-x-d+z}$$

$$\text{Or, } y_2 = \frac{L-x-d+z}{L-x} * y_C$$



ILD for BM at C,  $M_C$

## 5.10 Most critical position of a load on a beam span

[C] A train of point loads  
(ii) Maximum BM at a section

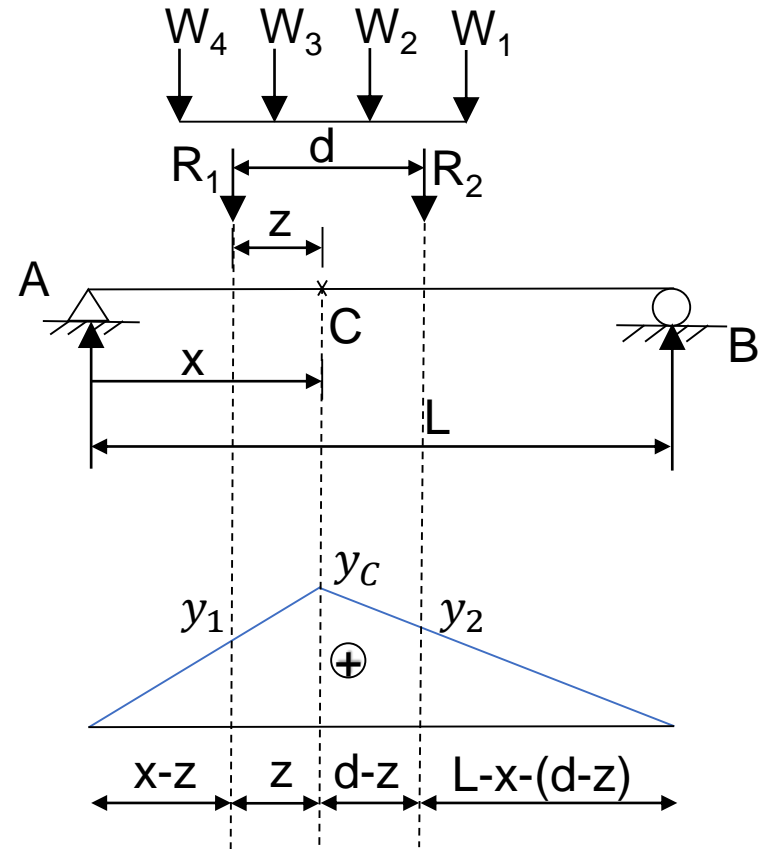
$$\begin{aligned}\therefore M_C &= R_1 y_1 + R_2 y_2 \\ &= R_1 * \frac{x-z}{x} * y_C + R_2 * \frac{L-x-d+z}{L-x} * y_C\end{aligned}$$

For  $M_C$  to be maximum,

$$\frac{dM_C}{dz} = 0$$

$$\text{Or, } R_1 y_C \left( -\frac{1}{x} \right) + R_2 y_C \left( \frac{1}{L-x} \right) = 0$$

$$\text{Or, } \left( \frac{R_1 y_C}{x} \right) = \left( \frac{R_2 y_C}{L-x} \right)$$



ILD for BM at C,  $M_C$

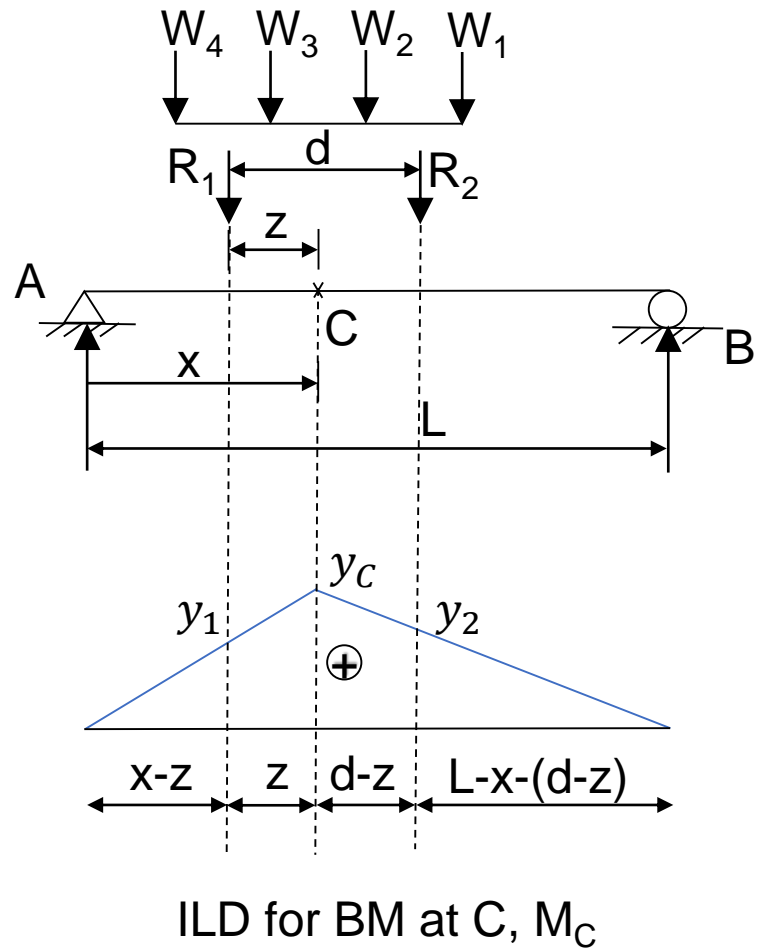
# 5.10 Most critical position of a load on a beam span

[C] A train of point loads  
 (ii) Maximum BM at a section

$$Or, \left(\frac{R_1 y_C}{x}\right) = \left(\frac{R_2 y_C}{L-x}\right)$$

$$Or, \left(\frac{R_1}{x}\right) = \left(\frac{R_2}{L-x}\right)$$

Hence, the average load on the left-side portion of the beam is the same as the average load on the right-side portion of the beam.



-----End of Lecture#9-----

-----End of Part III of III for Chapter5-----

# References

[1] Bhavikatti, S. S. (2011). *Structural Analysis –I* (4<sup>th</sup> ed.). New Delhi: Vikas Publishing House.