



# Course: Regulation and control

**Lecture 13:** Controller Design II – Compensators

**Lecturer:** Chalachew Werku

# Course Outline & Learning Objectives

- Understand the limitations of PID control.
- Learn frequency-domain design using Bode plots.
- Master the design of Lead and Lag Compensators.

## Recap: Limitations of PID

- PID is a "one-size-fits-most" solution.
- What if we need precise shaping of the closed-loop response?
- What if the performance requirements are very specific?

# Introducing Compensators

- Idea: Design a controller  $G_c(s)$  with a specific frequency-domain purpose.
- We can "shape" the open-loop frequency response  $G_c(s)G(s)$  to meet precise stability and performance specs.

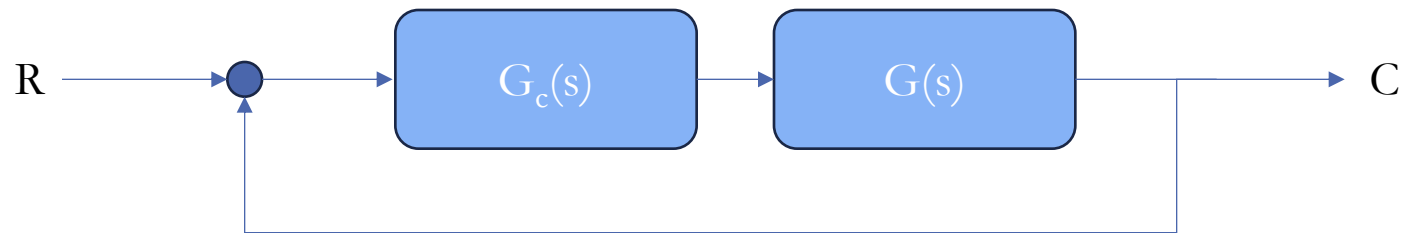


Fig 1: Closed-loop system with compensator [1]

# The Design Platform: Bode Plots

- Review:
  - **Magnitude Plot:** dB vs.  $\log(\omega)$
  - **Phase Plot:** Degrees vs.  $\log(\omega)$

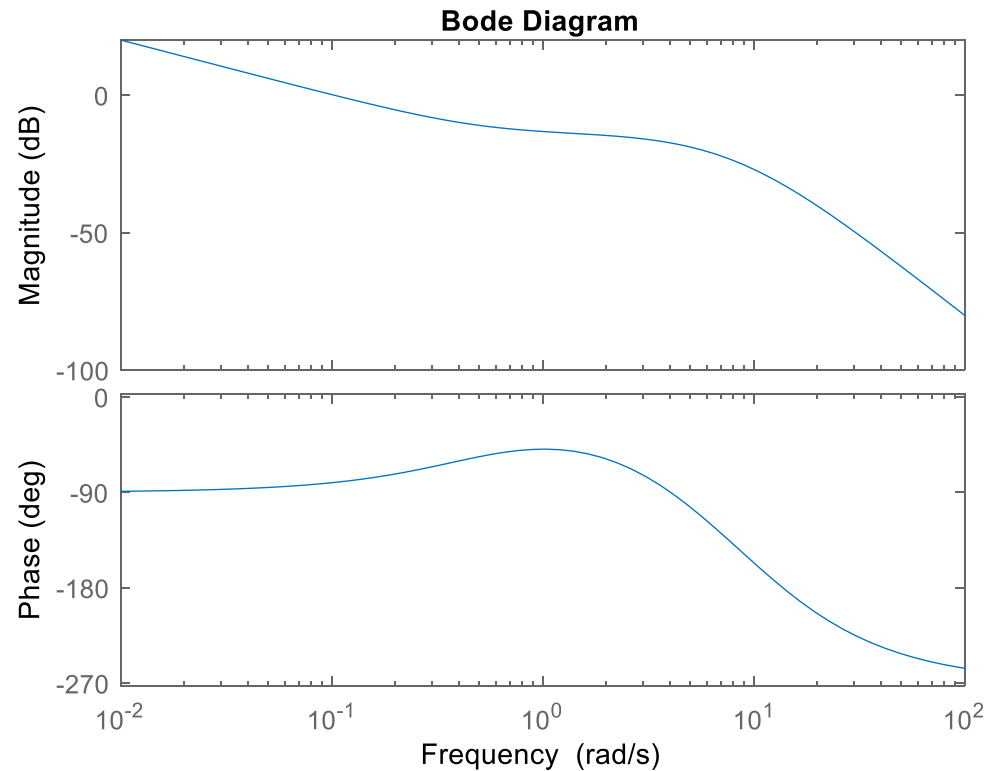


Fig 2: Bode plot, Magnitude vs Phase plot [2]

# Recap Gain Margin (GM) and Phase Margin (PM)

- **Gain Margin (GM):** How much gain can increase before instability.
- **Phase Margin (PM):** How much phase lag can increase before instability.
- Indicators of Robustness.

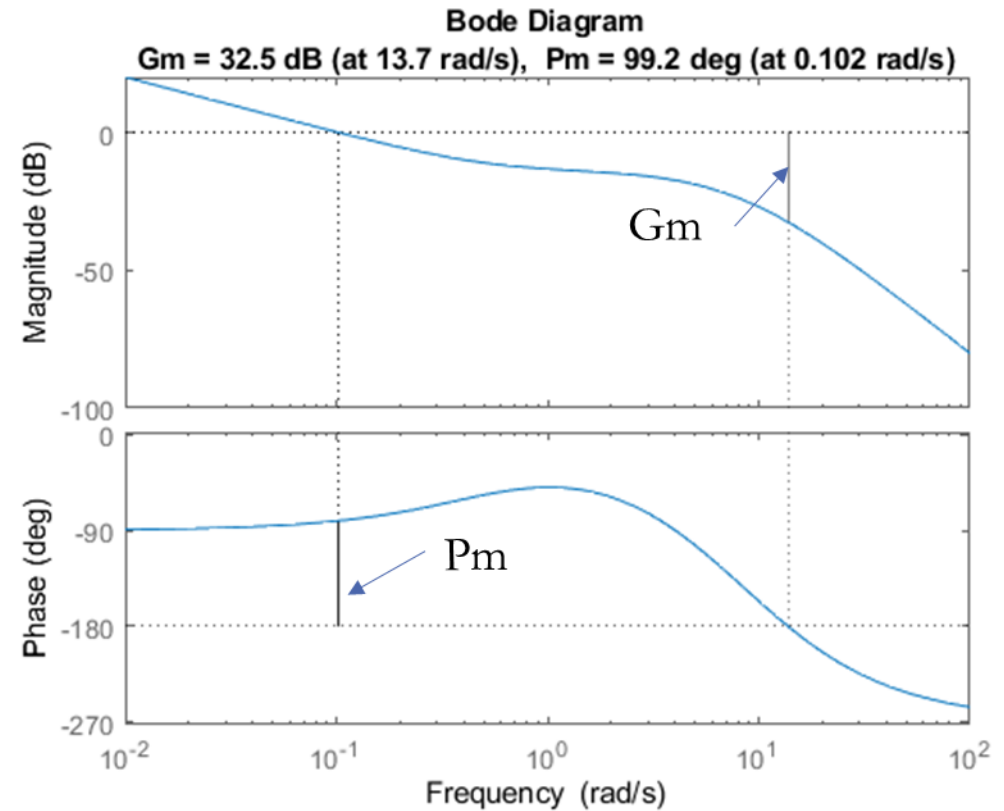


Fig 3: Gain margin vs Phase margin [3]

# Relating GM/PM to Time Response

- Higher Phase Margin  $\rightarrow$  Less Overshoot
- Higher Gain Crossover Frequency ( $\omega_{gc}$ )  $\rightarrow$  Faster Response

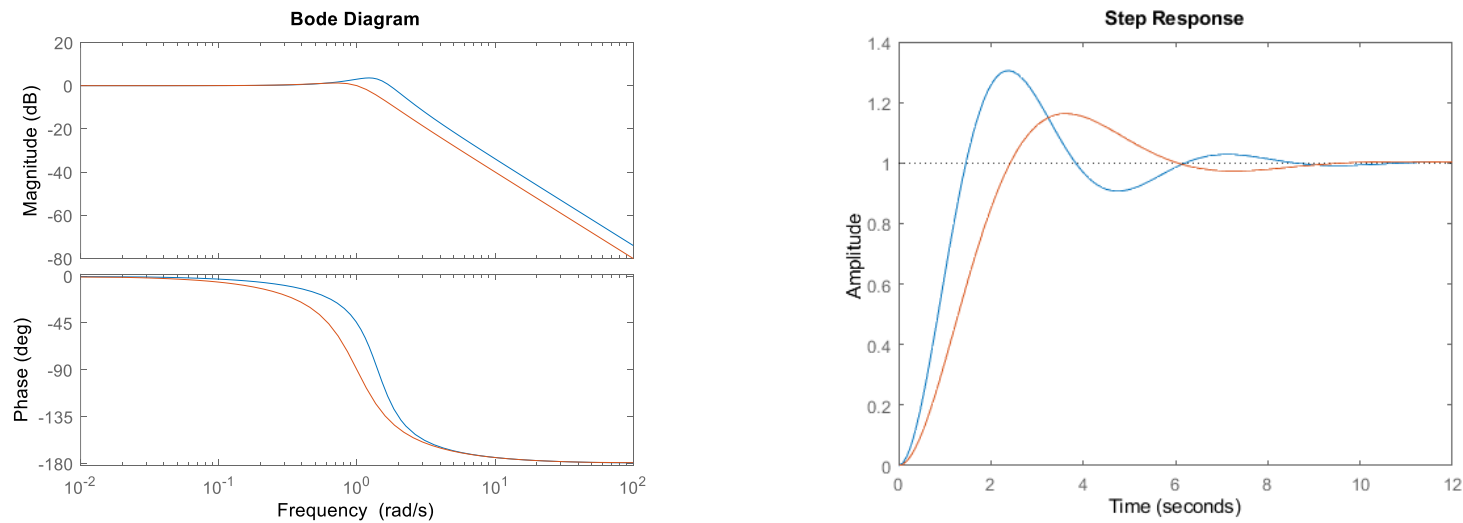


Fig 4: Frequency vs time response of a system [4]

# The Concept of "Loop Shaping"

- We design the compensator  $G_c(s)$  so that the open-loop transfer function  $L(s) = G_c(s)G(s)$  has a desirable Bode plot.
- We "shape" the  $L(s)$  curve to achieve desired PM,  $\omega_{gc}$ , and steady-state error.
- Un-compensated
- Compensated

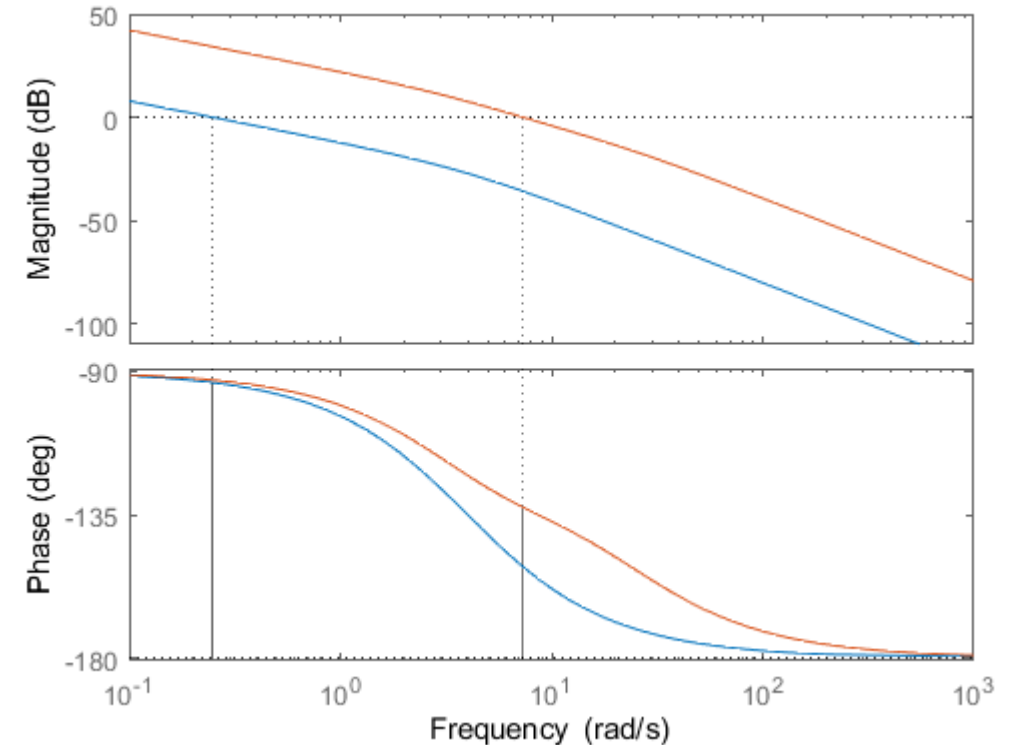


Fig 5: Loop-shaping (bode plot) [5]

# Performance Specifications in Frequency Domain

- **Desired Phase Margin (PM):** For sufficient damping (e.g.,  $PM > 45^\circ$ ).
- **Gain Crossover Frequency ( $\omega_{gc}$ ):** For desired speed.
- **Steady-State Error:** Dictated by low-frequency gain (e.g., high gain for small error).

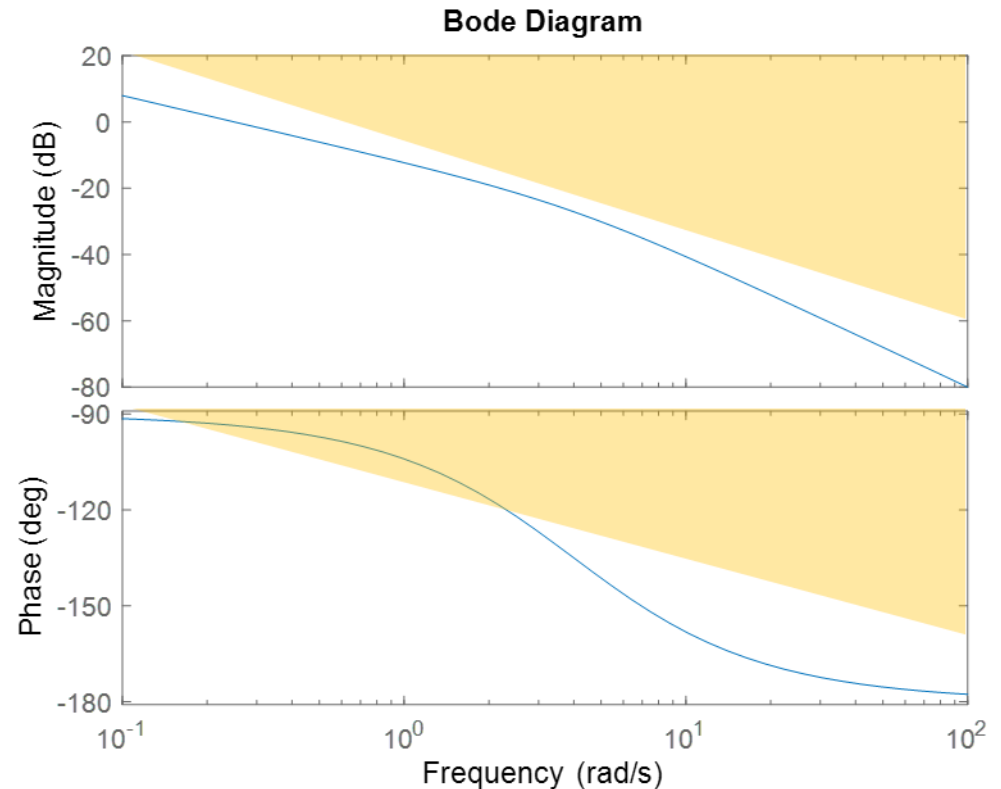


Fig 6: Desired region in bode plot [6]

# The General Form of a Lead/Lag Compensator

$$G_c = K_c \frac{(s + z)}{s + p}$$

- The locations of the Zero ( $z$ ) and Pole ( $p$ ) define the type.
- **Lead Compensator:**  $|z| < |p|$  (Zero before Pole).
  - Adds positive phase  $\rightarrow$  Improves PM.
- **Lag Compensator:**  $|z| > |p|$  (Pole before Zero).
  - Increases low-frequency gain  $\rightarrow$  Reduces steady-state error.

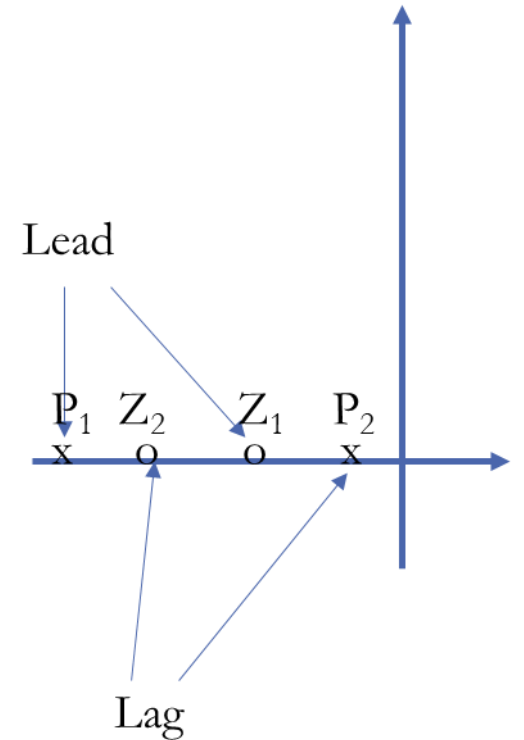


Fig 7: Pole and zero locations of compensators. [7]

## Quick Quiz

- For a compensator  $G_c(s) = \frac{s+1}{s+10}$ , is it a lead or a lag? Justify.

**Answer:**

*Lead. Because the zero is at  $s = -1$  and*

*the pole is at  $s = -10$ .*

$$|z| = 1 < |p| = 10.$$

# The Lead Compensator

- A lead compensator is a type of controller used in feedback control systems to improve the transient response (how fast the system responds) and stability.
- It does this by adding positive phase to the system's open-loop frequency response, effectively "pushing" the phase curve upward around the gain crossover frequency.
- The name "lead" comes from the fact that the output phase of the compensator leads the input phase for sinusoidal signals.

# Lead Compensator Goal

- **Primary Goal:** Improve Stability → Increase Phase Margin.
- **Secondary Goal:** Increase Speed → Raise Gain Crossover Frequency ( $\omega_{gc}$ ).

The Standard Form

- $G_c(s) = K_c \alpha \frac{sT+1}{\alpha sT+1}, 0 < \alpha < 1$ 
  - $\alpha$ : Determines the amount of phase lead.
  - T: Determines the frequency where max phase occurs.

# Bode Plot of a Standalone Lead Compensator

- **Magnitude:** High-pass filter characteristic.
- **Phase:** A "phase bump" centered at a specific frequency.

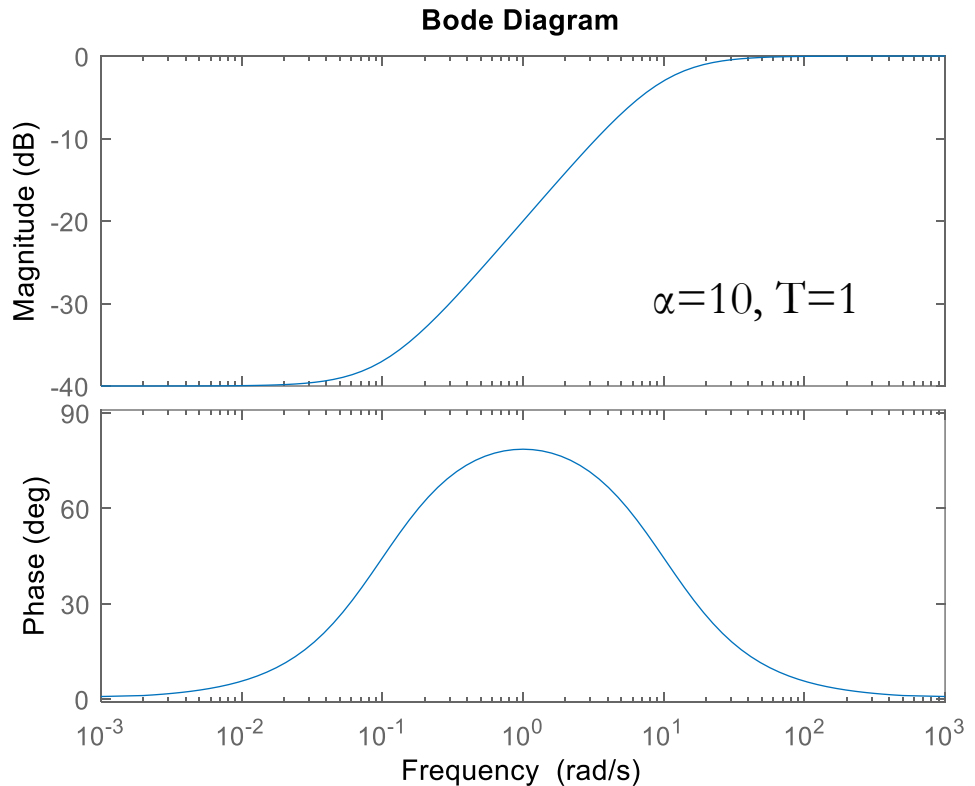


Fig 8: Standalone lead-compensator [8]

# Key Parameters

- **$\alpha$  (alpha)**: Sets the maximum phase lead  $\varphi_m$ . Larger  $\alpha \rightarrow$  larger  $\varphi_m$ .
- **T (Time Constant)**: Sets the frequency  $\omega_m$  where the max phase occurs.

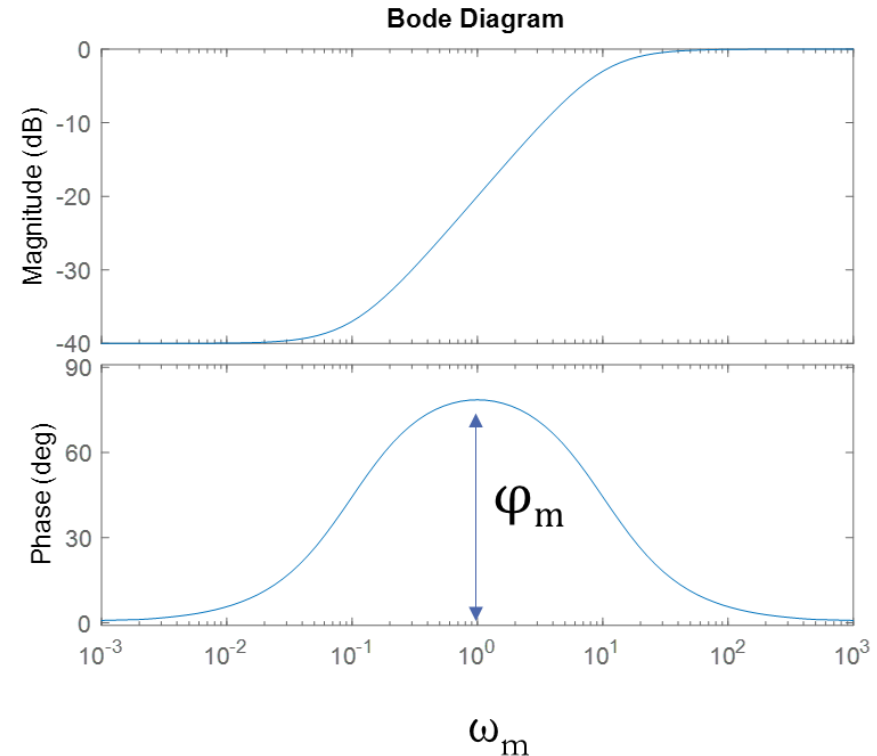


Fig 9: Key parameters on lead-compensator [9]

# Formula for Maximum Phase Lead and Frequency of Max Phase

## Maximum Phase Lead

$$\phi_m = \sin^{-1} \left( \frac{1 - \alpha}{1 + \alpha} \right)$$

- This is the maximum possible phase boost the compensator can provide

## Frequency of Max Phase

$$\omega_m = \frac{1}{\sqrt{\alpha T}}$$

- This is the center of the "phase bump".

# The Design Procedure for a Lead Compensator

- Step-by-Step List
  1. Determine required phase lead  $\varphi_m$ .
  2. Calculate  $\alpha$  from  $\varphi_m$ .
  3. Place  $\omega_m$  at the new gain crossover frequency.
  4. Determine  $T$  and then  $K_c$ .

# Step 1 and 2

## Step 1: Determine required $\phi_m$

- Required  $\varphi_m = \text{Desired PM} - \text{Current PM} + (5^\circ - 15^\circ \text{ Safety Factor})$
- The compensator must provide this extra phase.

## • Step 2: Calculate $\alpha$ from $\phi_m$

- Use the formula:  $\alpha = \frac{1 - \sin(\varphi_m)}{1 + \sin(\varphi_m)}$ 
  - Derived from  $\varphi_m = \sin^{-1} \left( \frac{1 - \alpha}{1 + \alpha} \right)$

## Step 3 and 4

Step 3: Place  $\omega_m$  at the new gain crossover frequency.

- Find the frequency where the uncompensated magnitude is  $1/\sqrt{\alpha}$ .
- This frequency will become the new  $\omega_{gc}$ , and we set  $\omega_m$  equal to it.

Step 4: Determine T and then K<sub>c</sub>

- From  $\omega_m = \frac{1}{T\sqrt{\alpha}}$ , calculate T.
- Set K<sub>c</sub> to achieve the required DC gain for steady-state error, or
- set or  $K_c\alpha=K$ ,  $K_c= 1$  initially and adjust if needed.

# Example 1

## *lead-compensator*

- Given:  $G(s) = 1 / s(s+2)$ 
  - Spec: Achieve  $PM \geq 85^\circ$ .

### *Solution*

From Bode plot of  $G(j\omega)$ , phase at gain crossover

$\omega_{gc} \approx 0.486 \text{ rad/sec}$  is about  $-103.7^\circ$ , so  $PM_{\text{current}} \approx 76.3^\circ$ .

### **Required additional phase lead:**

- $\phi_m = PM_{\text{des}} - PM_{\text{current}} + 5^\circ \approx 85 - 76.3 + 5 = 13.7^\circ$

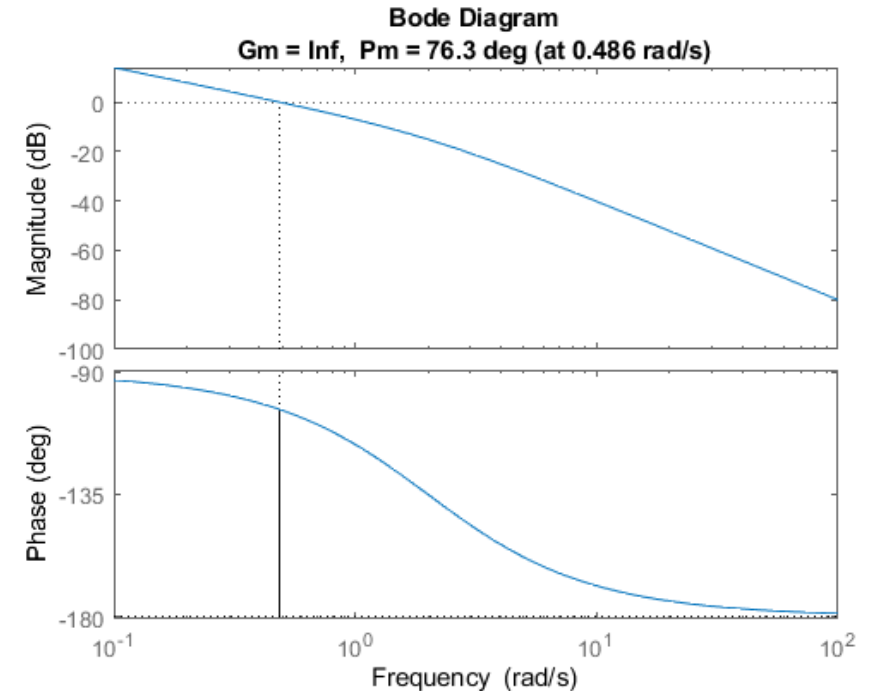


Fig 10: Uncompensated bode plot for example 1 [10]

# Example 1

*lead-compensator*

Cont....

Calculate  $\alpha$  from  $\varphi_m$

$$\alpha = \frac{1 + \sin\phi_m}{1 - \sin\phi_m} = \frac{1 + \sin 13.7^\circ}{1 - \sin 13.7^\circ} \approx 0.617$$

$\omega_{gc-new} = ?$

$$|G(j\omega_{gc-new})| = \frac{1}{\sqrt{a}} = \frac{1}{\omega\sqrt{\omega^2 + 4}} = 0.785, \quad \omega_{gc-new} = 0.626 \text{ rad/sec}$$

# Example 1

*lead-compensator*

Cont....

$$\omega_m = \frac{1}{T\sqrt{\alpha}}$$

$$\Rightarrow T = \frac{1}{\omega_m\sqrt{\alpha}} = \frac{1}{0.626 * \sqrt{0.617}} = 2.037$$

$$G_c(s) = K_c \alpha \frac{sT+1}{\alpha sT+1} \quad \text{setting } K_c \alpha = 1$$

$$= 1 * \frac{2.037s + 1}{0.617 * 2.037s + 1} = \frac{2.037s + 1}{1.257s + 1}$$

$$G_c(s)G(s) = \frac{2.037s+1}{1.257s+1} * \frac{1}{s(s+2)}$$

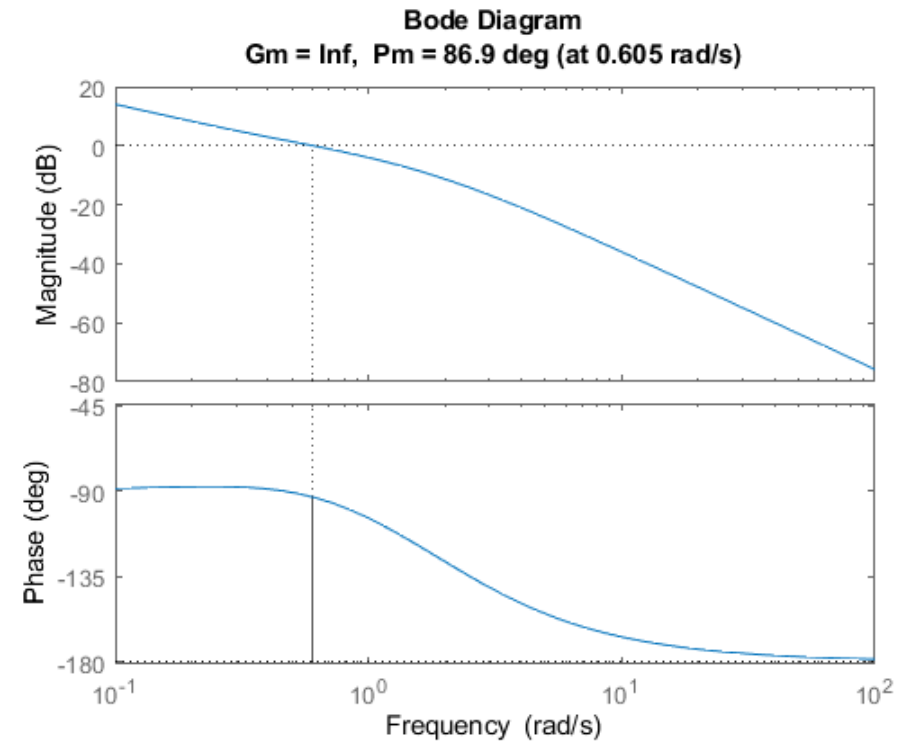


Fig 11: Compensated bode plot for example 1 [11]

# Summary of lead compensators

- **Effects on step response:** Reduced overshoot and faster settling time.
- **Limitations:** Amplifies high-frequency noise (due to its high-pass nature), Not effective for systems with already low phase margins at high frequencies.
- **We use it when:** more Phase Margin is needed, the system is too sluggish and you need a faster response, the system has excessive overshoot.

# The Lag Compensator

- A lag compensator is a type of controller used in feedback control systems to improve steady-state accuracy (reduce steady-state error) without significantly affecting the transient response.
- It does this by increasing the low-frequency gain of the open-loop system.
- The name "lag" comes from the fact that the output phase of the compensator lags behind the input phase for sinusoidal signals.

# Lag Compensator Goal

- Primary Goal → Improve Steady-State Accuracy.
- Secondary Goal → Allow for higher low-frequency gain without affecting stability.
- The Standard Form
  - $G_c(s) = K_c \beta \frac{Ts+1}{\beta Ts+1}, \beta > 1$
  - $\beta$ : Determines the amount of low-frequency gain boost.
  - T: Sets the corner frequency.

# Bode Plot of a Standalone Lag Compensator

- **Magnitude:** Low-pass filter characteristic. Gain is  $K_c$  at high frequency and  $K_c/\beta$  at low frequency.
- **Phase:** Adds negative phase (phase lag).

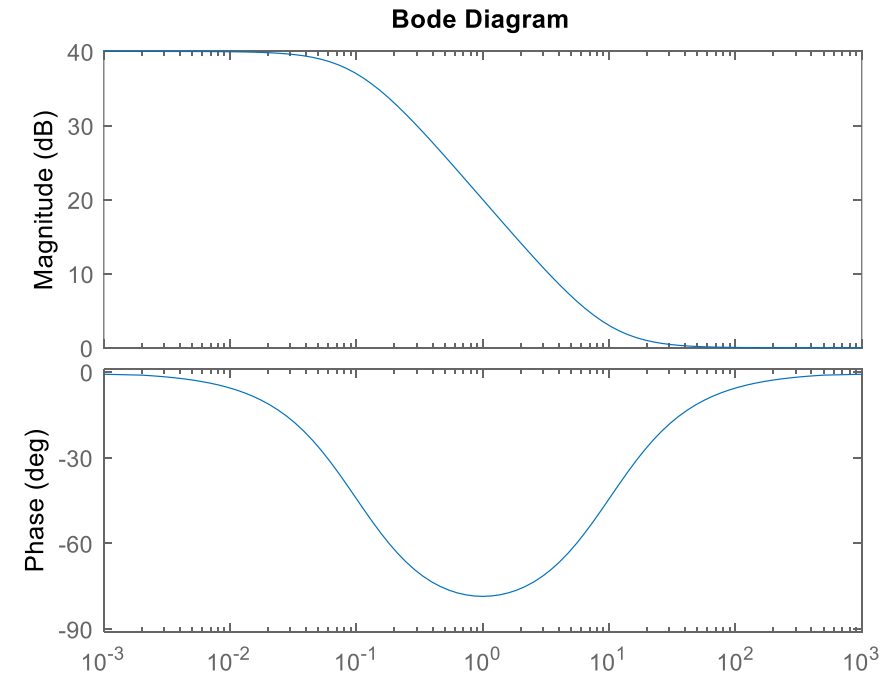


Fig 12: Standalone lag-compensator [12]

# Key Parameters

- $\beta$ - Sets the high-frequency attenuation

$$\frac{1}{\beta}$$

- The low-frequency gain boost.

$$\frac{K_c}{\beta}$$

- $T$ -Sets the frequency of the corner

$$\omega = \frac{1}{T} \text{ and } \omega_m = \frac{1}{T\sqrt{B}}$$

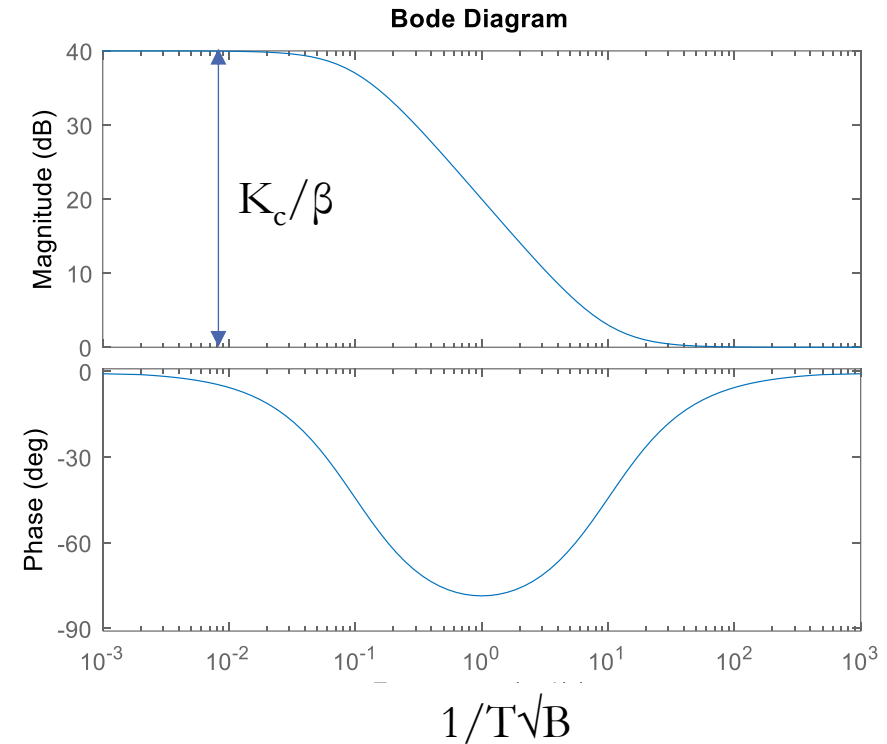


Fig 13: Key parameters on lag-compensator [13]

# The Design Procedure for a Lag Compensator

- Step-by-Step List:
  1. Determine  $K_c$  from steady-state error requirement.
  2. Plot Bode of  $K_c * G(s)$ , find frequency where PM is Spec PM + Safety.
  3. Place lag zero/pole well below this new crossover.
  4. Determine  $\beta$  from required attenuation.

# Step 1: Determine $K_c$ from SSE

- Use error constants:  $K_p$ ,  $K_v$ ,  $K_a$ .

SSE ( $e_{ss}$ )	Static error constants
$\frac{1}{1 + K_p}$	$K_p = \lim_{s \rightarrow 0} G(s)$
$\frac{1}{K_v}$	$K_p = \lim_{s \rightarrow 0} sG(s)$
$\frac{1}{K_a}$	$K_p = \lim_{s \rightarrow 0} s^2 G(s)$

- e.g., For ramp input,  $K_v = \lim_{s \rightarrow 0} sG(s)$  and  $e_{ss} = 1/K_v$  Set  $K_c$  to achieve the required  $K_v$ .

## Step 2 and 3

### Step 2: Find New Crossover with Safety

- Plot  $L(s) = K_c * G(s)$ .
- Find frequency  $\omega_{gc\_new}$  where  $\text{Phase} = -180^\circ + (\text{Desired PM} + 5^\circ - 15^\circ)$ .
- This safety factor accounts for the phase lag added by the compensator

### Step 3: Place Zero and Pole

- Place the zero at  $\omega_z = 1/T = 0.1 * \omega_{gc\_new}$ .
- This ensures the lag compensator adds minimal phase lag at the new crossover frequency.
- The pole is then at  $\omega_p = 1/(\beta T)$ .

## Step 4: Determine $\beta$

- At  $\omega_{gc\_new}$ , the uncompensated gain  $|K_c G(j\omega_{gc\_new})|$  must be attenuated to 0 dB.
- So, set

$$\beta = \frac{1}{|K_c G(j\omega_{gc\_new})|}$$

## Example 2

### *lag compensator*

- Design a lag compensator for a unity feedback system where the plant is:

$$G(s) = K/s(s+2)$$

- Design Requirements:
  - Steady-State Error:  $e_{ss} \leq 0.05$  for a unit ramp input.
  - Phase Margin:  $PM \geq 45^\circ$ .

## Example 2

*lag compensator: Solution*

Step 1: Determine the Required Gain  $K$  from the  $e_{ss}$  Specification

Steady-state error for a Type 1 system is  $e_{ss} = \frac{1}{K_v}$

$$K_v = \lim_{s \rightarrow 0} s \left[ \frac{K}{s(s+2)} \right] = \frac{K}{2}$$

$$e_{ss} = 1/K_v = 0.05 \rightarrow K = 40$$

$$G(s) = \frac{40}{s(s+2)}$$

## Example 2

*lag compensator: Solution*

Cont. . . .

Step 2: Find New Crossover with Safety

$$PM_{\text{uncomp}} = 18$$

$$\angle G(j\omega_{gc\text{new}}) = -180 + (PM_{\text{Desired}}) + (\text{Safety}) = -180 + 45 + 10 = -125$$

$$\angle G(j\omega) = -90 - \tan^{-1}(\omega/2) = -125$$

$$\omega_{gc\text{new}} = 1.40 \text{ rad/sec}$$

$$\frac{1}{\beta} * |G(j\omega_{gc\text{-new}})| = 1 \Rightarrow \beta = |G(j\omega_{gc\text{-new}})| = 11.7 \approx 12$$

## Example 2

### *lag compensator: Solution*

Step 3: Place Zero and Pole

Place the zero at  $\omega_z = 1/T$

$$= 0.1 * \omega_{gc\_new} = 0.14 \rightarrow T = 7.14$$

- The pole is then at  $\omega_p = 1/(\beta T)$

$$\rightarrow 1/(12 * 7.14) = 0.0117$$

$$G_c(s) = \frac{7.14s + 1}{85.7s + 1}$$

$$G_c(s)G(s) = \frac{7.14s + 1}{85.7s + 1} * \frac{40}{s(s + 2)}$$

Cont. . . .

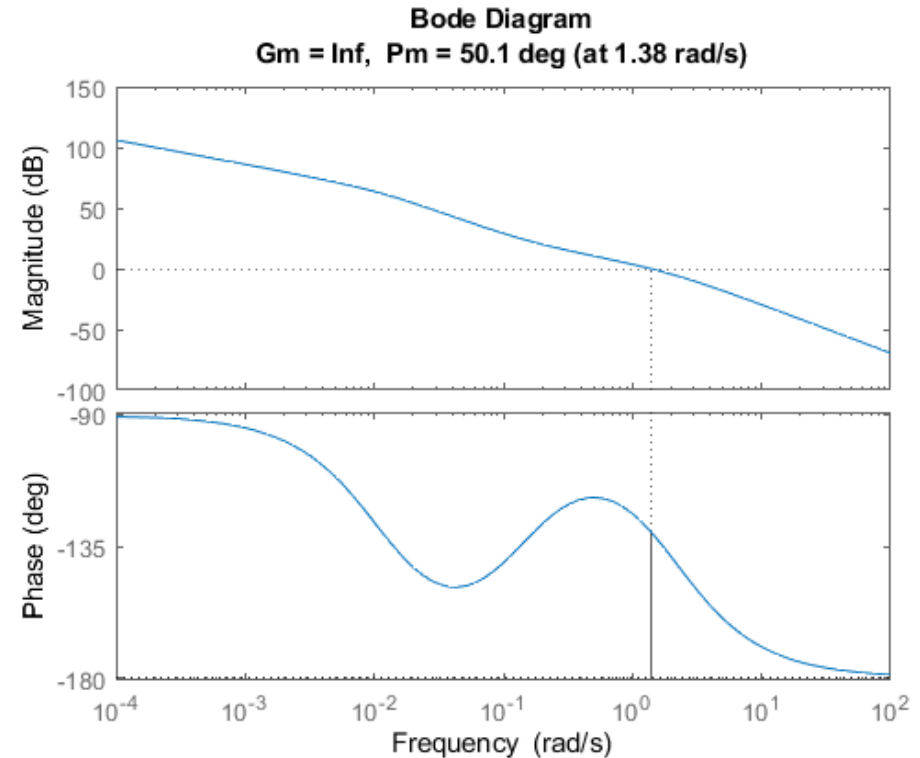


Fig 14: Compensated bode plot for example 2 [14]

# Summary of lag compensators

- **Effects on Step response:** Same or similar overshoot, Slower settling time and Drastically reduced steady-state error.
- **Limitations:** Slows down the system response and Can make the system more sluggish.
- **We use it when:** steady-state error is the primary concern and the transient response is acceptable but needs better accuracy.

# Lead-Lag Compensators

- Combines the benefits of both.
  - **Lead Part:** Speeds up response and improves PM.
  - **Lag Part:** Improves steady-state accuracy.

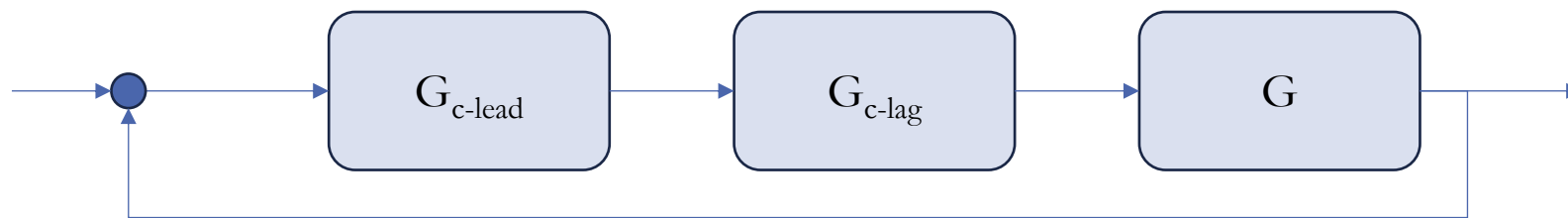


Fig 15: Closed-loop system with lead-lag compensator [15]

# Comparison Table

<b>Feature</b>	<b>Lead Compensator</b>	<b>Lag Compensator</b>
<b>Main Goal</b>	Improve Stability/Speed	Improve Steady-State
<b>Effect on BW</b>	Increases	Decreases
<b>Effect on PM</b>	Increases	Slight Decrease (managed)
<b>Noise</b>	Amplifies HF Noise	Attenuates HF Noise

# Summary & Key Takeaways

- PID is powerful but limited; compensators offer precise design.
- Lead: For Phase Margin and Speed. Use  $\alpha > 1$ .
- Lag: For Steady-State Error. Use  $\beta < 1$ .
- Design is done by shaping the Bode plot of the open-loop system.

# References

- [1] Chalachew Werku, 2025, Closed-loop system with compensator, Self-created
- [2] Chalachew Werku, 2025, Bode plot, Magnitude vs Phase plot, Self-created
- [3] Chalachew Werku, 2025, Gain margin vs Phase margin, Self-created
- [4] Chalachew Werku, 2025, Frequency vs time response of a system, Self-created
- [5] Chalachew Werku, 2025, Loop-shaping (bode plot), Self-created
- [6] Chalachew Werku, 2025, Desired region in bode plot, Self-created
- [7] Chalachew Werku, 2025, Pole and zero locations of compensators, Self-created
- [8] Chalachew Werku, 2025, Standalone lead-compensator, Self-created
- [9] Chalachew Werku, 2025, Key parameters on lead-compensator, Self-created
- [10] Chalachew Werku, 2025, Uncompensated bode plot for example 1, Self-created
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